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Heartbeat electro-language: Exploring piezoelectric technologies for cardiovascular health monitoring

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Blood flow
status

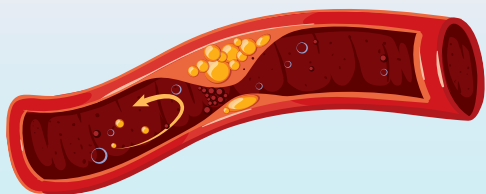


Heart rate

Pulse
waveform



Respiratory



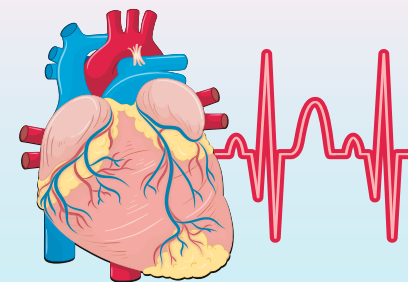
Arteriosclerosis



Blood pressure



Heart failure



Arrhythmia

1 **Heartbeat electro-language: Exploring piezoelectric**
2 **technologies for cardiovascular health monitoring**

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23

24 **Abstract**

25 Cardiovascular diseases remain the leading cause of global morbidity and mortality,
26 underscoring the urgent need for advanced technologies capable of continuous,
27 noninvasive, and intelligent monitoring. Piezoelectric sensors, owing to their inherent
28 electromechanical transduction, high sensitivity, and self-powered operation, offer a
29 compelling pathway for next-generation cardiovascular health monitoring. In this

30 review, we summarize recent advances in piezoelectric materials, from zero- to three-
31 dimensional architectures, and their integration into wearable and implantable
32 platforms. Key applications include the assessment of arterial health via pulse wave
33 velocity and vascular stiffness, cuffless blood pressure estimation, and the monitoring
34 of cardiopulmonary functions such as heart rate, respiratory rhythm, and cardiac
35 acoustics. We also highlight emerging strategies such as passive wireless
36 communication enabled by surface acoustic wave principles, and the development of
37 multimodal systems that concurrently capture mechanical, optical, and chemical signals.
38 The convergence of piezoelectric technologies with artificial intelligence and Internet
39 of Things frameworks enables real-time signal processing, remote access, and
40 personalized medical interventions. Finally, we discuss current challenges in material
41 biocompatibility, encapsulation, signal fidelity, and clinical translation, and outline
42 future directions for advancing high-performance piezoelectric systems for intelligent
43 cardiovascular diagnostics and connected healthcare.

44 **Keywords**

45 Cardiovascular monitoring; Piezoelectric effect; Flexible pressure sensor; Self-
46 powered devices; AI-enabled monitoring

47

48 **1. Introduction**

49 Cardiovascular diseases (CVDs), encompassing conditions such as coronary
50 artery disease, arrhythmias, hypertension, and stroke, pose one of the most critical
51 public health challenges globally [1-3]. According to the World Heart Federation's
52 *World Heart Report 2023*, CVDs were responsible for approximately 20.5 million
53 deaths in 2021, accounting for 31% of all global mortality and ranking as the leading

54 cause of death. These statistics underscore the urgent need for early diagnosis,
55 continuous monitoring, and precision interventions [4].

56 Driven by aging populations and changes in lifestyle, the incidence and burden of
57 CVDs have been steadily rising, with increasingly complex epidemiological patterns
58 [5, 6]. The progression and outcome of CVDs are influenced by a range of factors,
59 including genetic predisposition, environmental exposure, socioeconomic status, and
60 behavioral habits. Addressing this multifactorial challenge requires a holistic approach
61 that integrates personalized risk profiling, environmental context, and targeted medical
62 strategies [7, 8].

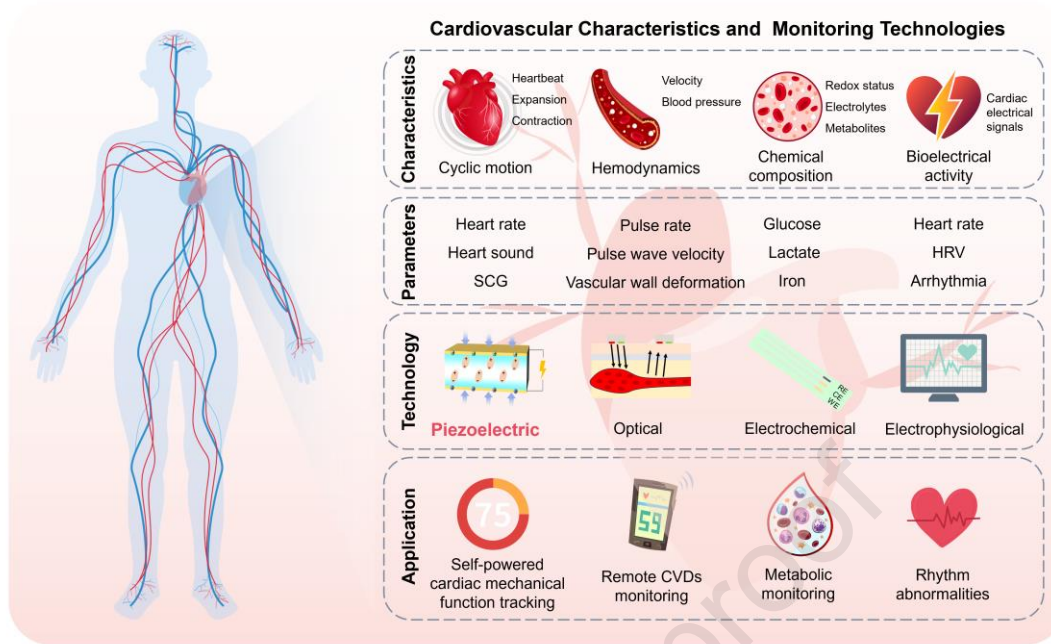
63 Real-time, high-fidelity monitoring plays a vital role in improving cardiovascular
64 outcomes by facilitating early detection, reducing the likelihood of acute events, and
65 enhancing survival and quality of life [9, 10]. Functional assessment of cardiovascular
66 health involves tracking cardiac and vascular mechanical activity such as heartbeat,
67 contraction, and expansion, alongside hemodynamic indicators (blood pressure, shear
68 stress, blood flow velocity), biochemical markers (oxygen saturation, glucose, lactate),
69 and electrical signals such as electrocardiograms [11]. To support such
70 multidimensional sensing, a variety of technologies have been developed, including
71 mechanical [12], optical [13], electrochemical [14], and electrophysiological methods
72 [15] (**Fig. 1**).

73 Conventional systems such as electrocardiography (ECG) and Holter monitors
74 provide high diagnostic accuracy for electrical abnormalities but are constrained by
75 rigid electrodes and external power supplies, limiting their long-term wearability and

76 adaptability to dynamic environments [16-18]. Photoplethysmography (PPG) often
77 suffers from motion artifacts and environmental interference, while force-based sensors,
78 such as piezoresistive and capacitive types, may exhibit baseline drift, low sensitivity,
79 and high energy consumption.

80 In contrast, piezoelectric sensors offer several advantages, including high
81 sensitivity to micro-mechanical deformations, fast response, mechanical flexibility, and
82 self-powered operation, making them particularly suitable for long-term, continuous
83 cardiovascular monitoring across multiple parameters [19, 20]. These devices also
84 enable remote data transmission and support personalized interventions for timely
85 clinical decision-making [21] (**Table 1**). As a result, the development of compact, high-
86 performance piezoelectric monitoring systems has emerged as a central focus of
87 cardiovascular sensing research [22].

88 Overall, piezoelectric technology offers a robust and scalable platform for
89 capturing subtle cardiovascular mechanical signals with high precision and energy
90 efficiency. Its seamless integration with flexible materials and emerging electronics,
91 combined with advances in nanotechnology, positions it as a promising solution for
92 real-time monitoring, early diagnosis, and personalized cardiovascular care in future
93 healthcare systems.



94

95 **Fig. 1.** Cardiovascular characteristics, monitoring parameters, and enabling technologies for
 96 health management. Overview of key cardiovascular features, including cyclic motion,
 97 hemodynamics, chemical composition, and bioelectrical activity. Corresponding physiological
 98 parameters such as heart rate, pulse wave velocity, and vascular deformation are monitored
 99 using piezoelectric, optical, electrochemical, and electrophysiological technologies. These
 100 approaches support applications in self-powered functional tracking, remote cardiovascular
 101 disease monitoring, metabolic analysis, and rhythm disorder detection.

102

103 2 Fundamentals of piezoelectric cardiovascular sensing

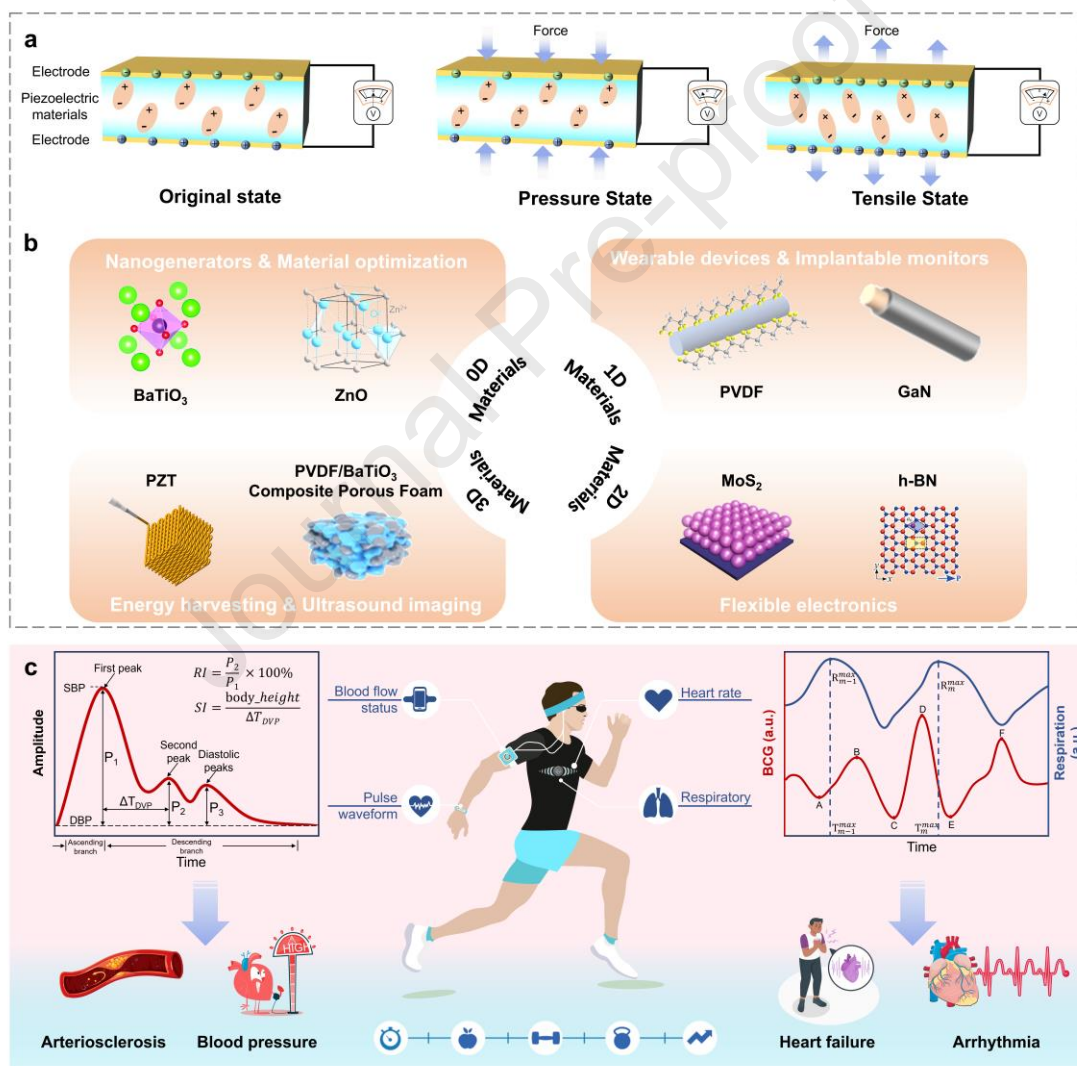
104 2.1 Mechanistic principles and material systems

105 The piezoelectric effect refers to the generation of electric charges on the surface
 106 of non-centrosymmetric materials when subjected to mechanical stress, resulting from
 107 polarization changes within their crystal lattice (**Fig. 2a**) [23-25]. This bidirectional
 108 transduction, which is mechanical-to-electrical (direct effect) and electrical-to-
 109 mechanical (inverse effect), forms the basis for both sensing [26, 27] and energy
 110 harvesting applications [28, 29]. In cardiovascular health monitoring, piezoelectric
 111 materials enable real-time, energy-efficient, and highly sensitive detection of

112 mechanical signals generated by cardiac and vascular activity. These include pulse
113 wave propagation, arterial wall deformation, and cardiac contractile motion, which are
114 closely linked to hemodynamic parameters such as blood pressure (BP), vascular
115 stiffness, and myocardial function.

116 Piezoelectric materials can be classified into four structural categories: zero-
117 dimensional (0D), one-dimensional (1D), two-dimensional (2D), and three-
118 dimensional (3D), each offering distinct advantages in sensitivity, flexibility,
119 biocompatibility, and device integration (**Fig. 2b**) [30, 31]. 0D materials such as ZnO
120 and BaTiO₃ nanoparticles exhibit high surface-to-volume ratios and interfacial
121 tunability, which enhance charge transfer and compatibility with flexible matrices [32,
122 33]. Other 0D candidates, such as quantum dots and halide perovskites, enable
123 multimodal signal coupling through enhanced local fields and optoelectronic
124 interactions [34]. 1D materials, including PVDF nanofibers and gallium nitride (GaN)
125 nanowires, offer superior mechanical compliance and directional electromechanical
126 response [35-38]. PVDF fibers show strong responses to subtle pulse deformations,
127 while GaN nanowires offer stable outputs for implantable biosensing [39, 40]. 2D
128 materials such as monolayer MoS₂ and hexagonal boron nitride (h-BN) exhibit in-plane
129 piezoelectricity due to the absence of inversion symmetry at the atomic scale [41-43].
130 Their ultrathin geometry, flexibility, and electronic functionality support integration
131 into conformal, wearable, and vascular-interfacing devices. Additional 2D candidates,
132 such as MXenes, also offer promising performance due to their high conductivity and
133 tunable surface chemistry [44]. 3D materials, including PZT (lead zirconate titanate)

134 ceramics and porous PVDF/BaTiO₃ composites, exhibit strong piezoelectric coupling
 135 and mechanical robustness, making them well-suited for energy harvesting, and
 136 ultrasound-driven applications [45-47]. Architected foams and negative Poisson's ratio
 137 structures further enhance deformation sensitivity [48, 49], while metal-organic
 138 frameworks (MOFs) expand possibilities for lightweight, tunable, and potentially
 139 degradable piezoelectric platforms.



140

141 **Fig. 2.** Fundamentals, materials, and applications of piezoelectric technology for
 142 cardiovascular monitoring. (a) Schematic of the piezoelectric effect under compressive
 143 and tensile stress. (b) Representative piezoelectric materials spanning 0D to 3D
 144 configurations for applications in energy harvesting, flexible electronics, and bio-
 145 integrated devices. Reproduced with permission [32]. Copyright 2012, Royal Society

146 of Chemistry. Reproduced with permission [33]. Copyright 2016, WILEY-VCH.
147 Reproduced with permission [37]. Copyright 2024, Elsevier. Reproduced with
148 permission [38]. Copyright 2019, Elsevier. Reproduced with permission [41].
149 Copyright 2019, Elsevier. Reproduced with permission [42]. Copyright 2012, American
150 Chemical Society. Reproduced with permission [45]. Copyright 2020, Elsevier.
151 Reproduced with permission [46]. Copyright 2021, American Chemical Society. (c)
152 Schematic of a multimodal wearable and implantable piezoelectric system for real-time
153 cardiovascular and cardiopulmonary monitoring. Pulse waveform features such as
154 stiffness index (SI) and reflection index (RI), along with ballistocardiogram (BCG) and
155 respiration signals, enable assessment of BP, arteriosclerosis, heart failure, and
156 arrhythmia.

157

158 These dimensional categories exhibit complementary advantages and limitations,
159 as summarized in **Table 2**. 0D materials excel in nanoscale integration but often suffer
160 from mechanical fragility. 1D systems are suitable for conformal wearables but may
161 face long-term stability challenges. 2D materials offer ultrathin, multifunctional sensing
162 interfaces, although issues of biocompatibility and manufacturing scalability remain
163 [50-52]. 3D architectures provide strong mechanical coupling and are well-suited for
164 implantable devices, energy harvesting, and ultrasound stimulation, especially when
165 developed with biocompatible or biodegradable matrices. Coordinated innovation
166 across all material dimensions will be essential for enabling long-term, personalized
167 cardiovascular monitoring.

168 As illustrated in **Fig. 2c**, piezoelectric systems integrated into wearable and
169 implantable platforms can capture multimodal signals, including arterial pulse
170 waveforms, BCG, and respiration patterns. These mechanical signals correlate with
171 physiological parameters such as systolic and diastolic blood pressure, SI, RI, cardiac
172 output, and respiratory rhythm. Such sensing capability supports early diagnosis and
173 dynamic tracking of hypertension, arteriosclerosis, heart failure, and arrhythmias.

174 Combined with wireless transmission and artificial intelligence (AI)-enabled data
175 processing, piezoelectric technologies offer a powerful foundation for next-generation
176 cardiovascular health management.

177

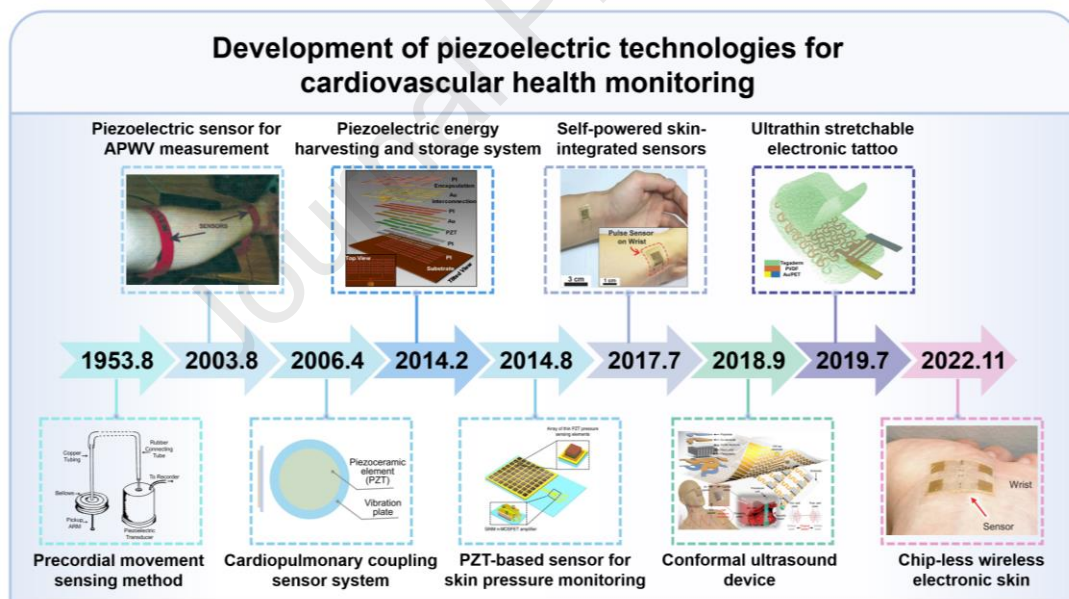
178 **2.2 Technological advances and evolution**

179 Piezoelectric technology, which converts mechanical energy into electrical signals,
180 has emerged as a compelling solution for cardiovascular health monitoring (**Fig. 3**). In
181 1953, Eddleman et al. [53] first applied piezoelectric transducers to record chest wall-
182 induced pulse waves, laying the groundwork for later developments. In 1985, Karr et
183 al. [54] utilized PVDF-based transducers for cardiovascular parameter screening via
184 mechanical coupling. In 1991, Arbeille et al. [55] combined piezoelectric sensors with
185 Doppler systems to measure hemodynamic parameters, with clinical validation in
186 pregnancy and fetal hypoxia.

187 Advances in AI, wearable electronics, and Internet of Things (IoT) technologies
188 have since expanded the capabilities of piezoelectric systems for real-time, high-
189 precision monitoring [56-58]. In 2003, McLaughlin et al. [59] developed a dual-sensor
190 system to measure pulse wave velocity (PWV) and assess vascular stiffness. In 2006,
191 Sato et al. [60] introduced a PZT-based system for monitoring heart and respiratory
192 rates in anesthetized mice, employing custom analog and digital circuits to reduce
193 signal noise.

194 Significant progress was made in 2014 when Rogers et al. [61] designed an ultra-
195 thin, flexible PZT energy harvester for cardiac signal acquisition, capable of powering
196 pacemakers. They later integrated PZT with silicon nanomembranes to develop a non-

197 invasive arterial pulse wave sensor [62]. In recent years, Park et al. [63] introduced a
 198 self-powered piezoelectric pulse sensor for real-time arterial pulse monitoring, while
 199 Wang et al. [64] incorporated ultra-thin piezoelectric ultrasonic transducers to enable
 200 skin-adherent devices for deep vascular BP monitoring. Further innovations include a
 201 highly flexible electronic tattoo platform by Ha et al. [65] in 2019, and a 2022 chip-less
 202 wireless electronic skin system based on GaN, developed by Kim [66], that enables
 203 passive signal acquisition without rigid integrated circuits. Together, these milestones
 204 mark the evolution of piezoelectric systems from basic mechanical sensors to intelligent,
 205 miniaturized platforms that are central to the future of cardiovascular diagnostics and
 206 digital health.



207
 208 **Fig. 3.** Milestones in the development of piezoelectric technologies for cardiovascular
 209 health monitoring. Chronological overview of key innovations in piezoelectric-based
 210 cardiovascular monitoring devices from 1953 to 2022. The timeline includes early
 211 mechanical sensing of precordial movements, cardiopulmonary coupling systems,
 212 energy-harvesting and self-powered skin sensors, PZT-based pressure monitors,
 213 conformal ultrasonic devices, and the latest chip-less wireless electronic skin platforms.
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 215 Reproduced with permission [59]. Copyright 2003, IOP Publishing. Reproduced with
 216 permission [60]. Copyright 2006, Springer Nature. Reproduced with permission [61].

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218 Nature. Reproduced with permission [63]. Copyright 2017, WILEY-VCH. Reproduced
219 with permission [64]. Copyright 2018, Springer Nature. Reproduced with permission
220 [65]. Copyright 2019, WILEY-VCH. Reproduced with permission [66]. Copyright
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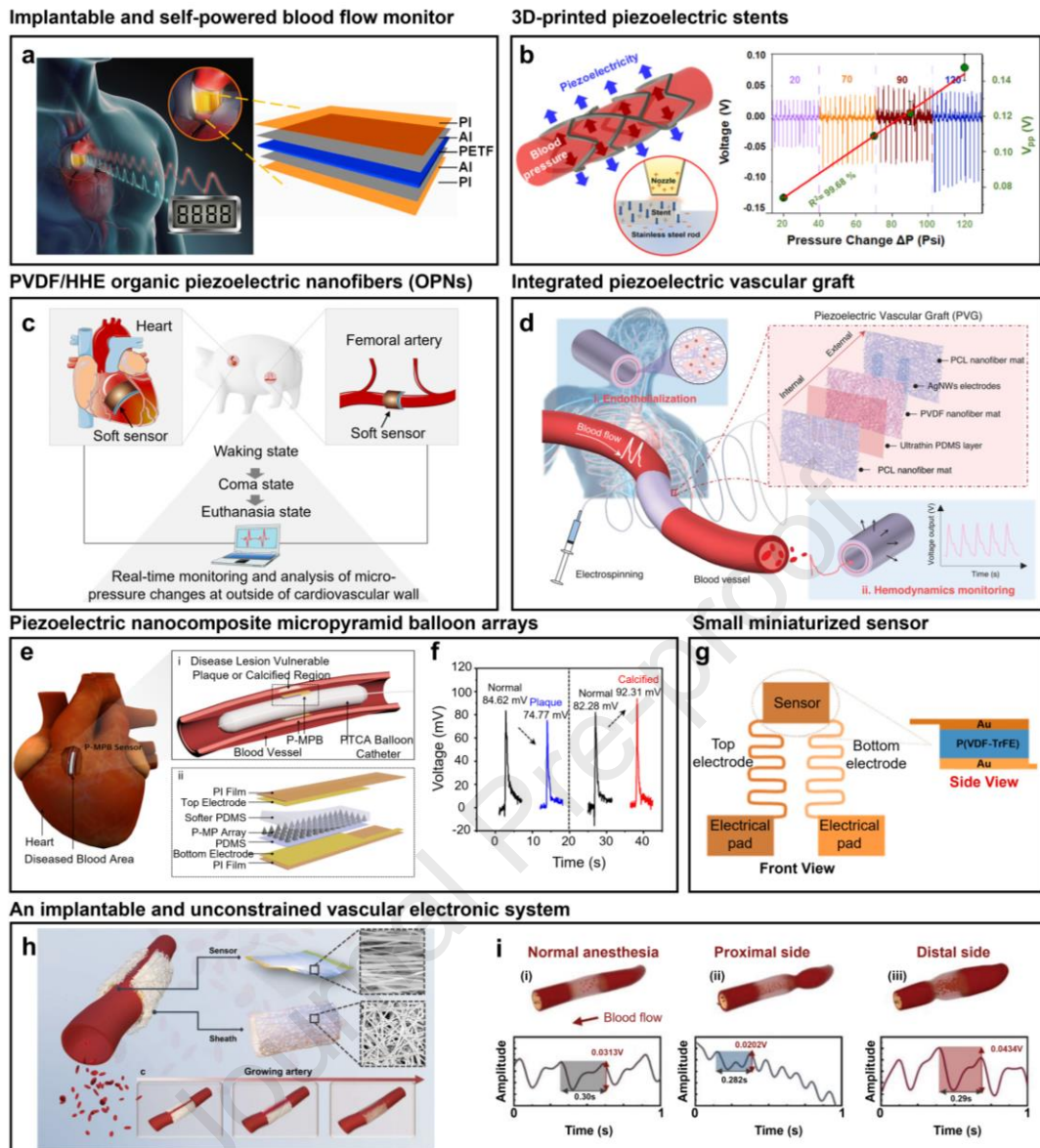
222

223 **3 Applications in cardiovascular monitoring**

224 **3.1 Hemodynamic-based arterial health assessment**

225 **3.1.1 Implantable sensors**

226 Over the past two decades, implantable electronic systems have shown
227 considerable advantages for continuous hemodynamic monitoring and in vivo
228 therapeutic applications [67]. Cheng et al. [68] developed a self-powered and visualized
229 monitoring system based on a 200 μm polarized PVDF piezoelectric thin film. The
230 device, wrapped around the ascending aorta of a pig, harvested biomechanical energy
231 and provided real-time feedback on blood flow status with high linearity ($R^2 > 0.99$)
232 and sensitivity (173 mV/mmHg), significantly outperforming previous devices (**Fig.**
233 **4a**). Expanding on structural integration, Pan et al. [69] reported a piezoelectric vascular
234 stent featuring a sawtooth geometry, fabricated via FDM-based 3D printing with
235 embedded electric fields. Composed of sodium potassium niobate and PVDF-HFP, the
236 device demonstrated stable voltage output under simulated pressure fluctuations and
237 offered reliable pressure sensitivity for intravascular sensing (**Fig. 4b**).



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Fig. 4. Implantable piezoelectric sensors for arterial health monitoring. (a) Multilayer implantable sensor for self-powered blood flow monitoring. Reproduced with permission [68]. Copyright 2016, Elsevier. (b) 3D-printed piezoelectric stent for real-time pressure sensing and hemodynamic analysis. Reproduced with permission [69]. Copyright 2024, American Chemical Society. (c) Soft PVDF/HHE piezoelectric nanofiber sensor for monitoring cardiovascular micro-pressure changes across physiological states. Reproduced with permission [70]. Copyright 2019, American Chemical Society. (d) Integrated piezoelectric vascular graft (PVG) featuring electrospun nanofibers for enhanced endothelium compatibility and continuous hemodynamic monitoring. Reproduced with permission [71]. Copyright 2024, WILEY-VCH. (e) Piezoelectric micro-pyramid balloon sensor for detecting pressure changes in diseased vessels. (f) Output voltage signals from different lesion types under balloon compression. Reproduced with permission [72]. Copyright 2023, American Chemical Society. (g) Schematic of a miniaturized piezoelectric force sensor with vertical and planar electrode configurations. Reproduced with permission [73]. Copyright 2020,

254 American Chemical Society. (h) Conceptual illustration of an unconstrained vascular
255 electronic system with sheath-assisted implantation. (i) Representative pulse
256 waveforms from a stenosed artery model under different anesthesia and positional
257 conditions. Reproduced with permission [74]. Copyright 2024, WILEY-VCH.
258

259 In pursuit of enhanced performance and biocompatibility, Li et al. [70] designed
260 core-shell PVDF/HHE nanofibers with aligned β -phase nanocrystals. The resulting
261 soft piezoelectric sensor was capable of capturing micro-pressure variations on
262 cardiovascular walls with high sensitivity. Implanted into a pig model, it accurately
263 reflected variations in vascular elasticity and pathological states such as conduction
264 blocks and thrombus formation (**Fig. 4c**). Further integrating sensing and tissue
265 regeneration functions, Ma et al. [71] developed a piezoelectric vascular graft using
266 electrospun PVDF/PCL nanofibers. This graft supported real-time hemodynamic
267 monitoring while maintaining favorable mechanical properties and endothelialization,
268 offering a promising platform for long-term vascular health tracking (**Fig. 4d**). Chang
269 et al. [75] demonstrated a self-powered implantable pressure sensor by embedding ZnO
270 nanofillers into PVDF nanofibers, achieving stable performance when adhered to
271 cardiovascular tissues such as the heart and femoral artery, and enabling real-time
272 tracking of vascular condition changes.

273 In the context of localized vascular assessment, Kang et al. [72] introduced a
274 piezoelectric micro-pyramid balloon catheter (p-MPB) sensor. Featuring
275 microstructured piezoelectric arrays on a balloon surface, this device enabled direct
276 measurement of vascular stiffness in coronary arteries. Ex vivo experiments on pig
277 hearts confirmed its ability to distinguish mechanical variations in diseased tissues,
278 supporting its potential for the early diagnosis of vascular pathologies such as

279 atherosclerosis and aneurysms (**Figs. 4e, f**). To support catheter-based intraoperative
280 feedback, Gil et al. [73] designed a force sensor incorporating a P(VDF-TrFE) layer for
281 integration at the tip of medical catheters. The sensor enabled real-time monitoring of
282 vascular contact pressure, which is critical for preventing endothelial damage and fluid
283 leakage during surgical procedures (**Fig. 4g**). Toward adaptive long-term monitoring,
284 Tang et al. [74] proposed an unconstrained vascular electronic system composed of
285 fixed piezoelectric sensors embedded in a growable sheath. Implanted around
286 developing arteries in rabbits, the system wirelessly recorded hemodynamic signals and
287 captured pathological changes such as stenosis and retrograde blood flow, indicated by
288 attenuated or distorted pulse waveforms (**Figs. 4h, i**). Several biologically compatible
289 and degradable materials have been found to exhibit excellent piezoelectric responses
290 [76, 77]. Cheng et al. [78] fabricated a fully organic force sensor using amino acid
291 crystal films and polyaniline electrodes encapsulated in PLA. The device exhibited
292 excellent stability and a broad detection range, offering suitability for long-term in vivo
293 monitoring of physiological pressures.

294 Collectively, these advances demonstrate the growing versatility of implantable
295 piezoelectric systems for enabling the real-time, high-sensitivity assessment of arterial
296 function and hemodynamic status, laying a foundational framework for in vivo
297 diagnosis and intervention in cardiovascular diseases.

298 **3.1.2 Wearable sensors**

299 Wearable piezoelectric sensors provide a noninvasive, low-power, and continuous
300 means of capturing subtle arterial wall deformations, enabling real-time assessment of

301 vascular mechanical properties. By analyzing pulse wave signals collected from
 302 superficial arteries, such devices can extract surrogate indicators of arterial stiffness,
 303 offering early insights into vascular aging and arteriosclerosis [79-81]. Due to the
 304 significantly higher arterial hardness of patients with arteriosclerosis, features extracted
 305 based on pulse signals can be easily used to diagnose the disease, such as the time delay
 306 between P_1 and P_2 (Δt_{DVP}), the time delay between P_1 and P_3 (PPT), the PWV, the
 307 stiffness index (SI), and the radial augmentation index (AI_r) (**Fig. 2c**). The calculation
 308 methods for the indicators used in this work are as follows [82]:

$$309 \quad \Delta t_{DVP} = t_{p_2} - t_{p_1} \dots\dots\dots (1)$$

$$310 \quad PPT = t_{p_3} - t_{p_1} \dots\dots\dots (2)$$

$$311 \quad PWV = 0.8 \times \frac{2\Delta L}{\Delta t_{DVP}} \dots\dots\dots (3)$$

$$312 \quad SI = \frac{H}{PPT} \dots\dots\dots (4)$$

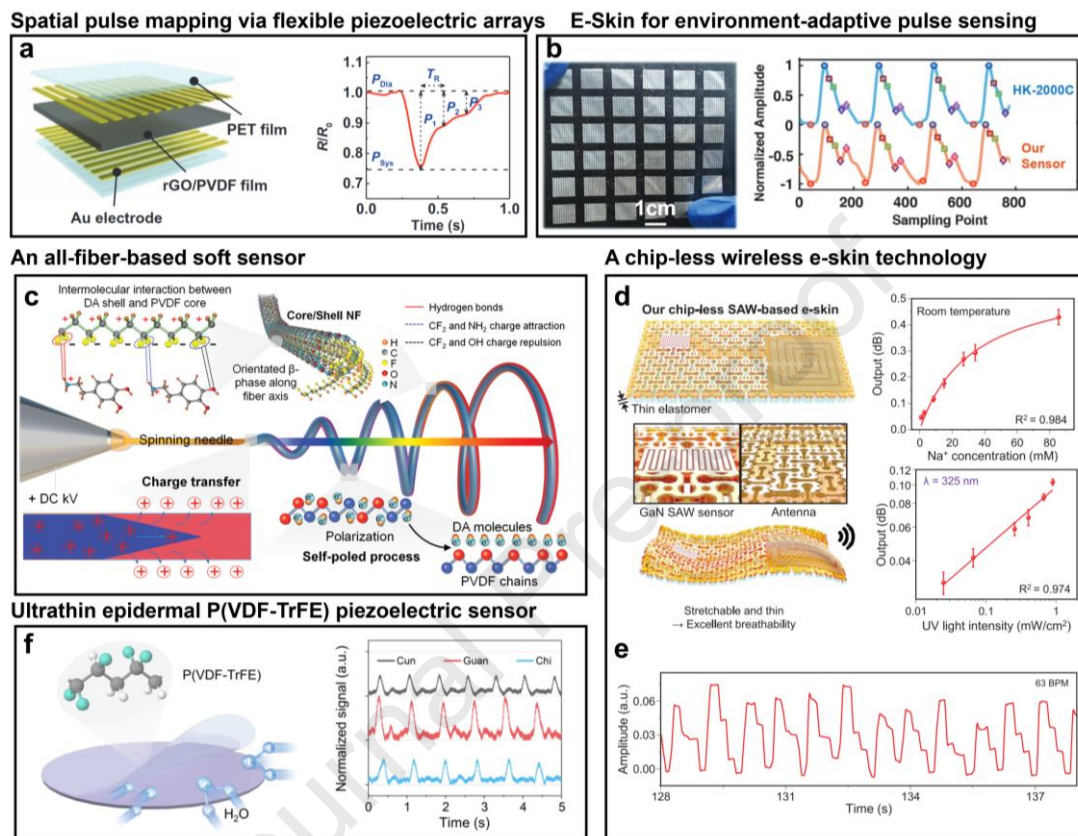
$$313 \quad AI_r = \frac{h_2}{h_1} \dots\dots\dots (5)$$

314 In equations (1, 2), t_{p1} , t_{p2} , and t_{p3} are the times corresponding to P_1 , P_2 , and P_3 ,
 315 respectively. In equations (3, 4), ΔL is the length from jugulum to symphysis, 0.8 is a
 316 recommended correction factor for international standardization, and H is the height of
 317 the tester [83]. In equation (5), h_1 and h_2 are the heights of P_1 and P_2 , respectively.

318 Park et al. [84] developed an e-skin based on microstructured PVDF composites,
 319 which allowed the continuous tracking of pulse dynamics with sensitivity to
 320 environmental changes, such as skin temperature fluctuations (**Fig. 5b**).
 321 Complementarily, Han et al. [85] proposed a high-density piezoelectric sensor array
 322 integrated into a flexible platform, enabling simultaneous detection and spatial mapping

323 of arterial and venous pulses (**Fig. 5a**). The system demonstrated strong signal fidelity
324 and temporal resolution, supporting the derivation of pulse features relevant to arterial
325 stiffness monitoring under practical wearable conditions. Li et al. [86] also developed
326 a flexible piezoelectric sensor comprising randomly stacked PVDF/DA nanofiber (NF)
327 thin films (**Fig. 5c**). The device conformed to various body surfaces (e.g., chest, neck,
328 and wrist), accurately capturing weak mechanical stimuli caused by blood pulsation.
329 Under different physiological states, the device demonstrated robust capabilities in
330 detecting diaphragm contractions and peripheral arterial wall changes with precision
331 and speed. To address the mechanical mismatch between conventional sensors and the
332 human epidermis, Kim et al. [66] innovatively reported a chip-free wireless electronic
333 skin based on surface acoustic wave (SAW) sensors, fabricated from ultra-thin,
334 freestanding single-crystal piezoelectric GaN films (**Fig. 5d**). This SAW-based
335 electronic skin enables highly sensitive, low-power, and long-term sensing of strain,
336 ultraviolet (UV) exposure, and ionic concentrations in sweat. Researchers demonstrated
337 pulse monitoring for up to one week (**Fig. 5e**), providing a cost-effective and versatile
338 platform for wireless health monitoring devices with low power consumption and high
339 sensitivity. Tian et al. [87] introduced an ultrathin, conformal piezoelectric device based
340 on a 3 μm P(VDF-TrFE) film, fabricated via spin-coating and aqueous exfoliation
341 techniques. The device exhibited excellent skin conformity and sensitivity, enabling
342 stable pulse waveform acquisition under dynamic conditions and across multiple
343 arterial sites (**Fig. 5f**). This work underscores the potential of skin-integrated
344 piezoelectric platforms for high-resolution, distributed vascular health monitoring in

345 wearable applications. These advances collectively underscore the growing potential of
 346 wearable piezoelectric systems for enabling high-resolution, noninvasive monitoring of
 347 arterial health.



348
 349 **Fig. 5.** Wearable piezoelectric sensors for arterial health monitoring. (a) Spatial pulse
 350 mapping using a flexible rGO/PVDF composite sensor array sandwiched between gold
 351 electrodes. Reproduced with permission [84]. Copyright 2015, American Association
 352 for the Advancement of Science. (b) Batch fabrication and performance evaluation of
 353 flexible environment-adaptive pulse sensors. Reproduced with permission [85].
 354 Copyright 2022, WILEY-VCH. (c) All-fiber PVDF/DA core-shell piezoelectric
 355 nanofibers fabricated via electrospinning, showing oriented β -phase formation induced
 356 by intermolecular interactions. Reproduced with permission [86]. Copyright 2021,
 357 WILEY-VCH. (d) Chip-less wireless e-skin platform based on GaN SAW sensors,
 358 responsive to Na^+ concentration and ultraviolet light intensity. (e) Wireless arterial pulse
 359 monitoring using the GaN SAW-based e-skin. Reproduced with permission [66].
 360 Copyright 2022, American Association for the Advancement of Science. (f) Schematic
 361 and signal output of an ultrathin P(VDF-TrFE) epidermal sensor fabricated via aqueous
 362 exfoliation. Reproduced with permission [87]. Copyright 2023, American Chemical
 363 Society.

364

365 In recent years, micromechanical ultrasonic transducers have found increasing
366 applications in medical fields, including volumetric ultrasound imaging [88] and
367 intravascular imaging [89], and they are now emerging as key components in wearable
368 systems for arterial stiffness monitoring. Jiang et al. [90] proposed a $1.5 \times 1.5 \text{ mm}^2$
369 array of 5 MHz piezoelectric micromachined ultrasonic transducers (PMUT) designed
370 for tracking radial artery wall motion. The complete ultrasonic measurement system
371 offers advantages such as compact size and low power consumption, demonstrating
372 significant potential for continuous cardiovascular health monitoring. Ding et al. [91]
373 developed a compact, low-power pulsed-wave Doppler flowmeter based on AlN
374 PMUTs, integrating custom electronics and a blood flow simulation system to achieve
375 real-time monitoring of flow velocity and direction. The device accurately captured
376 Doppler frequency and spectral changes linked to pulsatile flow, demonstrating
377 feasibility for vascular function assessment and future wearable applications. Gami et
378 al. [92] introduced a PMUT-based pulse wave imaging system for evaluating central
379 arterial mechanics in wearable and at-home settings. Compared to a clinical-grade
380 probe, the PMUT array achieved high accuracy in pulse wave velocity estimation (error
381 $<5\%$) and remained robust under noisy conditions, confirming its suitability for low-
382 power, high-precision arterial stiffness monitoring. These studies highlight the strong
383 potential of PMUT technology as a foundation for next-generation wearable systems
384 for continuous vascular health assessment.

385 **3.2 Cuffless BP monitoring**

386 Pulse wave characteristics are critical indicators for evaluating vascular health and

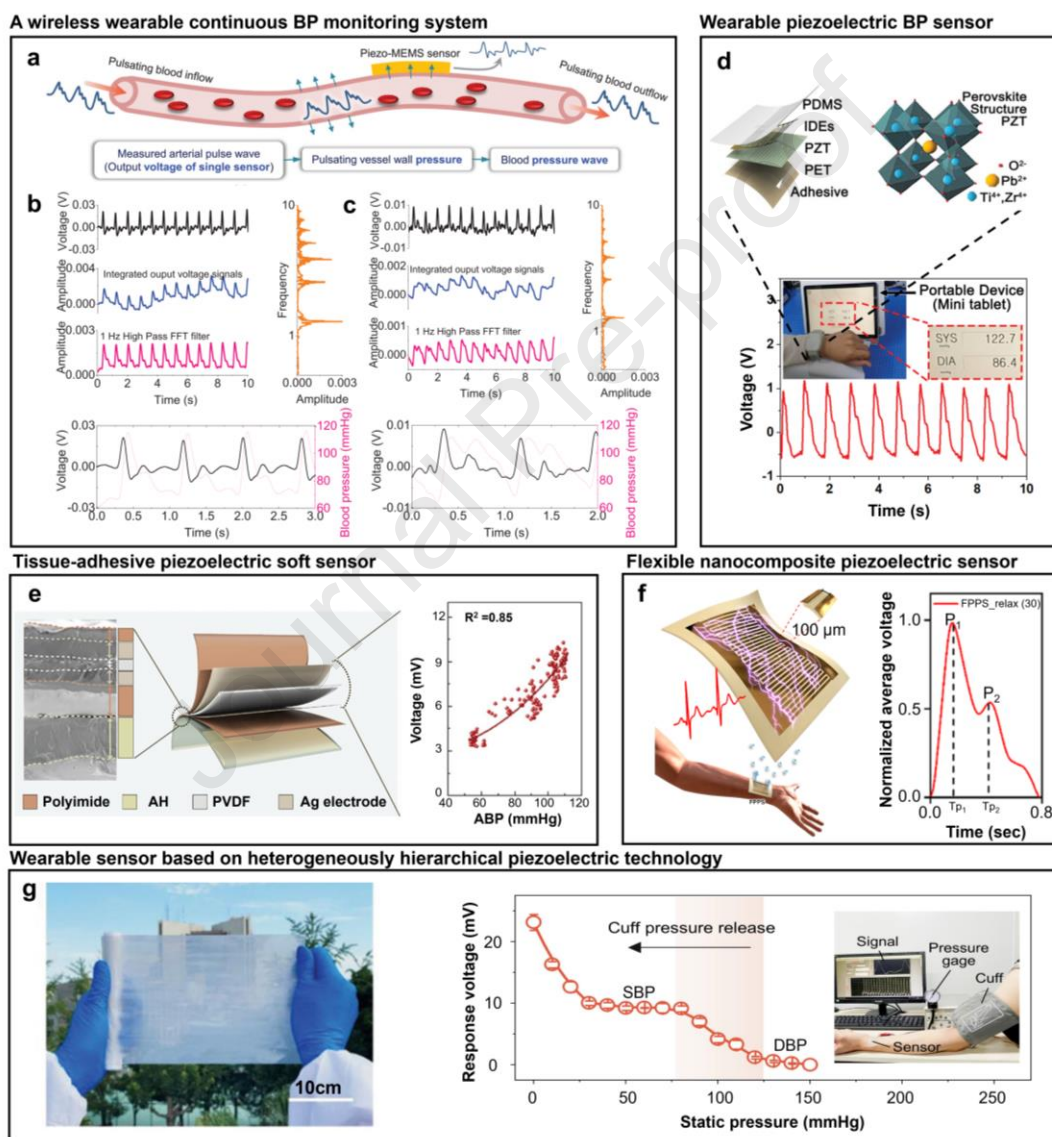
387 cardiovascular function. Key parameters, such as wave peaks and wave velocity, are
388 closely associated with BP, arterial stiffness, and vascular elasticity. In recent years,
389 piezoelectric technology has emerged as a core tool in pulse wave monitoring due to its
390 high sensitivity and rapid response capabilities.

391 Yi et al. [93] proposed a mathematical model for arterial pulse piezoelectric
392 dynamics (**Fig. 6a**), investigating the relationship between arterial BP waves and
393 piezoelectric arterial pulse waves across nano- to macro-scale functional layer
394 thicknesses. Their findings demonstrated the feasibility of using single and multiple
395 piezoelectric arterial pulse sensors to monitor BP (**Figs. 6b, c**). By advancing the
396 understanding of arterial pulse piezoelectric responses, these results contribute to the
397 development of portable, wearable, and continuous cardiovascular health monitoring
398 technologies.

399 **3.2.1 Single-site piezoelectric measurement**

400 Continuous monitoring of BP remains a considerable challenge due to the low
401 quality of the signal and the lack of an accurate transfer function to convert the sensor
402 signal to a BP value. Min et al. [94] developed an ultra-thin piezoelectric sensor
403 combining a PDMS passivation layer and a medical-grade adhesive layer, achieving
404 high sensitivity (0.062 kPa^{-1}), rapid response time (23 ms), and excellent mechanical
405 stability (**Fig. 6d**). Through mechanical loading tests exceeding 50,000 cycles, the
406 sensor demonstrated exceptional stability and consistency in both dynamic and static
407 environments. Wang et al. [95] developed a tissue-adhesive piezoelectric soft sensor
408 (TPSS) that integrates a mussel-inspired adhesive hydrogel layer with a flexible PVDF-

409 based piezoelectric architecture to enable real-time, continuous BP monitoring during
 410 cardiac surgery. The sensor exhibits excellent mechanical compliance, strong
 411 bioadhesion, and an ultrathin, lightweight form factor, allowing stable attachment to
 412 dynamic tissue surfaces such as the beating heart. In vivo experiments demonstrated
 413 high signal fidelity and strong agreement with catheter-based measurements (Fig. 6e).



414
 415 **Fig. 6.** Piezoelectric sensors for cuffless BP monitoring based on single-site pulse
 416 waveform analysis. (a) Schematic of arterial pressure transmission and sensing using a
 417 wearable piezoelectric sensor. (b, c) Pulse waveform acquisition from the finger and
 418 elbow using a cutaneous piezoelectric device, with corresponding signal processing and
 419 BP correlation. Reproduced with permission [93]. Copyright 2022, WILEY-VCH. (d)
 420 Structure and output of a flexible piezoelectric BP sensor integrated with a portable

421 device for wireless pulse signal transmission. Reproduced with permission [94].
422 Copyright 2023, WILEY-VCH. (e) SEM image and exploded view of a TPSS, revealing
423 its tightly bonded multilayer structure, which enables a clear correlation between
424 arterial BP and output voltage. Reproduced with permission [95]. Copyright 2023,
425 WILEY-VCH. (f) Schematic of a flexible nanocomposite piezoelectric sensor with
426 improved dispersion and permeability for high-fidelity pulse detection. Reproduced
427 with permission [96]. Copyright 2023, American Chemical Society. (g) Large-area
428 hierarchical piezoelectric composite film for cuffless monitoring of systolic/diastolic
429 pressure and real-time cardiovascular signals. Reproduced with permission [97].
430 Copyright 2024, WILEY-VCH.

431

432 Conductive fillers are favored for their unique interfacial polarization and
433 accompanying percolation effects, which bring new ways to achieve higher
434 piezoelectricity [98]. Inspired by the structure of muscle fibers, Su et al. [99] developed
435 a piezoelectric textile based on PDA-coated BTO (barium titanate) nanoparticles. The
436 incorporation of functional fillers enhanced interfacial polarization and percolation
437 effects, leading to a significant improvement in piezoelectric performance. The
438 resulting textile demonstrated high sensitivity in detecting pulse wave features,
439 enabling its use in BP and cardiovascular condition assessment. Similarly, Kim et al.
440 [96] embedded surface-functionalized PZT nanoparticles into a PVDF matrix (**Fig. 6f**),
441 which enhanced the interfacial polarization and percolation effects, thereby improving
442 the piezoelectric output. The fabricated flexible sensor exhibited high sensitivity for
443 pulse wave monitoring and is applicable for BP and vascular health evaluation. Tian et
444 al. [97] reported a wearable sensor based on heterogeneous layered piezoelectric
445 composites, fabricated using a scalable, non-equilibrium process combining
446 electrospinning and hot pressing. This process layered MXene and boron nitride (BN)
447 nanosheets within a poly(vinylidene fluoride-trifluoroethylene) [P(VDF-TrFE)] matrix,
448 referred to as PT in this study (**Fig. 6g**). The sensor continuously monitored

449 cardiovascular parameters and extracted pulse waveform data from detected signals,
450 which strongly correlated with clinical results. Long-term tracking experiments
451 validated its reliability, showcasing its potential for personalized healthcare
452 applications.

453 **3.2.2 Dual-site sensing and PWV estimation**

454 Pulse transit time (PTT) and PWV are two interdependent metrics that characterize
455 the temporal and spatial dynamics of arterial pulse propagation. PTT, defined as the
456 time for a pulse wave to travel between two arterial sites [100], is influenced by vascular
457 elasticity [101, 102] and has been widely used in arterial stiffness evaluation [103],
458 myocardial ischemia detection [104], and sleep monitoring [105]. PWV, calculated as
459 the ratio of travel distance to PTT, serves as a widely accepted index for arterial stiffness
460 and is strongly associated with cardiovascular risk [106-109]. These parameters,
461 derived from dual-site pulse sensing, provide complementary insights into vascular
462 compliance and circulatory health.

463 As early as 2006, Fool et al. [110] employed piezoelectric technology to detect
464 radial artery pulsations at the wrist, estimating PTT through experiments involving 17
465 healthy adults. This study demonstrated the exceptional performance of piezoelectric
466 sensors in capturing arterial pulse wave details, particularly for dynamic monitoring of
467 BP and arterial stiffness. With advances in technology, research has shifted toward more
468 precise and convenient monitoring devices. The development of data analytics has also
469 driven significant progress in pulse arrival time (PAT) research through ML techniques.
470 Liang et al. [111], analyzing data from the MIMIC database, found that PAT sensitivity

471 might decrease in individuals with a higher baseline BP, posing challenges to its broad
 472 applicability. Shao et al. [112] utilized deep learning (DL) models to extract complex
 473 features from large-scale PAT datasets for BP prediction and cardiovascular risk
 474 assessment. Compared to traditional linear models, DL methods demonstrate greater
 475 capability in managing multivariable interferences and uncovering latent patterns
 476 within complex data. Although PAT is closely related to dynamic BP changes, its
 477 efficacy as a BP-related parameter is influenced by various factors. Finnegan et al. [113]
 478 noted a negative correlation between PAT and BP, but high-load states such as exercise
 479 or emotional fluctuations may introduce additional confounding factors, including
 480 changes in cardiac preload, afterload, and peripheral resistance.

481 Continuous, cuffless, and non-invasive BP monitoring through the measurement
 482 of PWV is widely regarded as a promising technique for real-time cardiovascular
 483 assessment [114]. The Moens–Korteweg (MK) equation [115] and the Hughes equation
 484 [116] are commonly employed to establish a relationship between PWV and BP (P).

485
$$\text{MK Equation: } PWV = \sqrt{\frac{Eh_0}{2\rho R_0}} \dots\dots\dots(6)$$

486
$$\text{Hughes Equation: } E = E_0 \exp(\alpha P) \dots\dots\dots(7)$$

487 In equations (6, 7), E , h_0 , and R_0 represent the elastic (tangential) modulus under BP
 488 (P), arterial wall thickness, and arterial radius, respectively; ρ denotes blood density; E_0
 489 is the elastic modulus at zero BP; and α is a material coefficient of the artery. The MK
 490 equation assumes a thin arterial wall and fixed radius, which may not hold true for
 491 human arteries. Conversely, the Hughes equation is entirely empirical.

492 To address these limitations, Ma et al. introduced an improved formula for the

493 relationship between PWV and BP by incorporating the Fung hyperelastic model. This
494 formulation was further generalized to encompass both linear elastic and hyperelastic
495 materials, where α and β are determined by the material properties and geometric
496 characteristics of the arteries [117].

$$497 \quad P = \alpha \cdot PWV^2 + \beta \dots\dots\dots(8)$$

498 The PWV also can be derived from measurements of the pressure wave on two sites of
499 the arterial tree [118]. In equation (9), the time difference Δt between the arrival of the
500 pulse at each sensor position, together with the distance L between the two sensors,
501 allows the calculation of PWV:

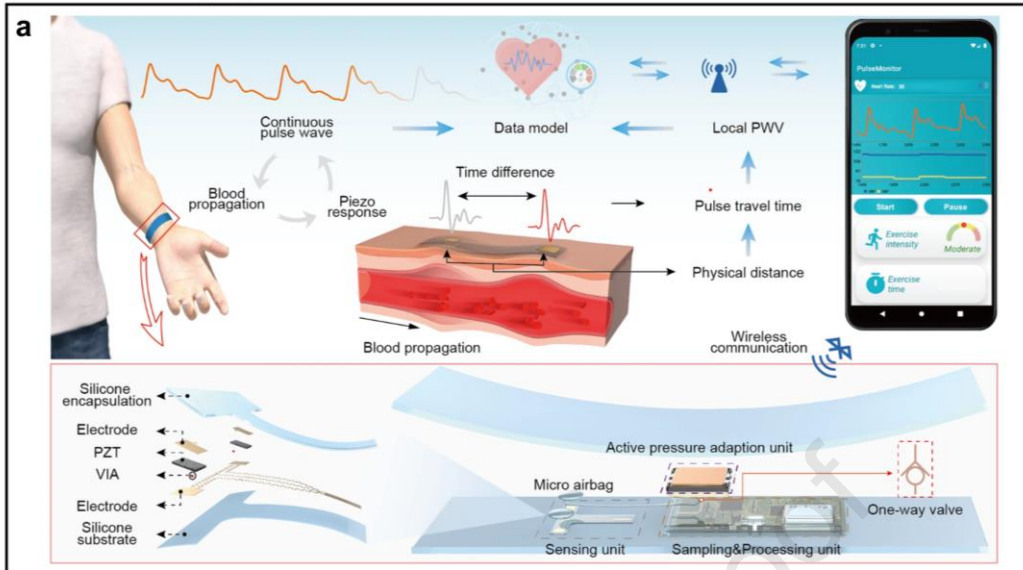
$$502 \quad PWV = \frac{L}{\Delta t} \dots\dots\dots(9)$$

503 Clinically, the gold standard for continuous BP monitoring involves the use of
504 fiber-based pressure sensors implanted at the arterial center [119, 120]. However, such
505 methods are highly invasive, increasing patient discomfort and infection risks,
506 rendering them unsuitable for routine monitoring. Li et al. [121] proposed a thin, soft,
507 miniaturized system (TSMS) comprising sensing, active pressure adaptation, and data
508 processing modules (**Fig. 7a**). Two piezoelectric sensors were used to calculate the local
509 PWV and combined with multiple pulse waveform features to establish a BP prediction
510 model. Through the XGBoost algorithm, the PWV and waveform features were mapped
511 to the BP, realizing high-precision and continuous noninvasive BP monitoring. Chen et
512 al. [122] developed a flexible piezoelectric pulse sensor (F-PPS) based on single-crystal
513 III-N thin films, capable of accurately measuring pulse waveforms and calculating
514 physiological parameters such as PTT across multiple arterial sites. The sensor offers

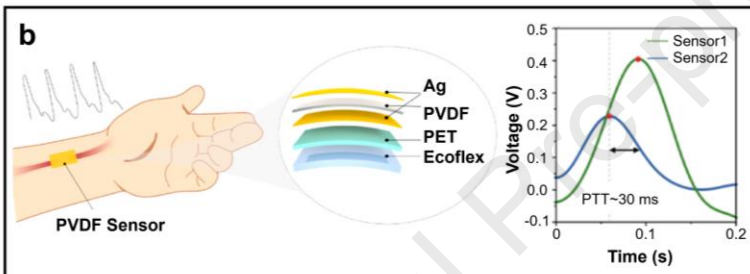
515 high sensitivity, noninvasiveness, and flexibility, enabling real-time detection of pulse
516 waveform changes and making it suitable for continuous cardiovascular health
517 monitoring. In addition to improving the sensitive materials and device structure used
518 to improve the output of piezoelectric sensors, adding an elastomer between the skin
519 and the piezoelectric layer can also improve the signal quality [123, 124]. Zhang et al.
520 [125] investigated the effects of elastic media with varying thicknesses and elastic
521 moduli on PVDF sensor performance. They identified an optimal piezoelectric pulse
522 sensor (PPS) based on PVDF film, integrated dual probes in the sensor, and verified a
523 stable mapping between PWV and BP by measuring local PWV at two locations at a
524 10 mm pitch, yielding predictions that were highly consistent with those of a
525 conventional electronic sphygmomanometer (**Fig. 7b**). Additionally, Okano et al. [126]
526 described a multimodal cardiovascular monitoring system that combines piezoelectric
527 sensors with other biosignal acquisition technologies. The system improves PWV
528 extraction accuracy through a cross-correlation algorithm and relies only on a dual-
529 sensor arrangement with 1–2 cm spacing, avoiding the dependence of traditional
530 methods on widely spaced measurement points (**Fig. 7c**). Nordine et al. [127] employed
531 a noninvasive system based on piezoelectric/piezo capacitive sensors (PES/PCS) to
532 capture dynamic changes in pulse transit time in a heterogeneous cohort of patients
533 undergoing major surgeries. This system innovatively uses a dual-sensor structure on
534 the wrist to simultaneously measure the pulse wave at two locations, and it accurately
535 extracts the PTT through a cross-correlation algorithm, which in turn calculates the
536 local PWV.

537 Arrhythmia induces hemodynamic changes in the arteries, which compromise the
538 accuracy of commercial electronic BP monitors [128]. Guo et al. [129] introduced a
539 PVDF-based piezoelectric sensor (**Fig. 7d**) capable of detecting ectopic beats from the
540 radial artery. Kaplan–Meier analysis also confirmed a positive correlation between
541 central PWV-related indices and recurrence risk, demonstrating a stable mapping
542 between PWV and BP status obtained by the dual-sensor approach, which can be used
543 to predict arrhythmic outcomes (**Fig. 7e**). Compared to traditional methods, this
544 approach demonstrates higher sensitivity and accuracy in identifying arrhythmias,
545 enabling real-time capture and analysis of PWV variations and offering new
546 possibilities for clinical applications. Obeid et al. [130] proposed a non-invasive
547 method for measuring central and peripheral PWV by combining piezoelectric sensors
548 with second derivative algorithms. Additionally, Guo et al. [131] developed a
549 multimodal device for cuffless BP measurement using a PVDF piezoelectric sensor
550 array and near-infrared spectroscopy (NIRS). This device calibrates a hemodynamics-
551 based PTT and BP model using arterial parameters, accounting for previously
552 overlooked factors in related studies and thereby reducing BP estimation errors.
553 Katsuura et al. [132] introduced pulse wave monitoring technology based on flexible
554 piezoelectric thin-film arrays, highlighting its advantages in real-time measurement
555 peak characteristics. Their study showed that the multi-point monitoring capability of
556 flexible arrays significantly enhances spatial resolution, facilitating regional vascular
557 condition assessments.

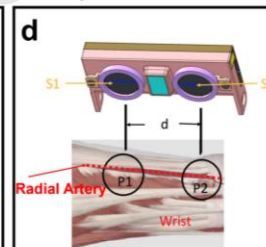
A folded double-layer piezoelectric sensor



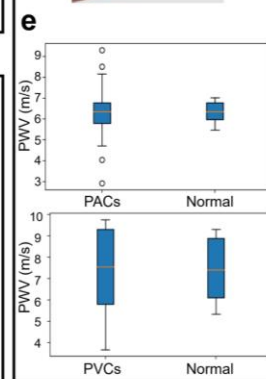
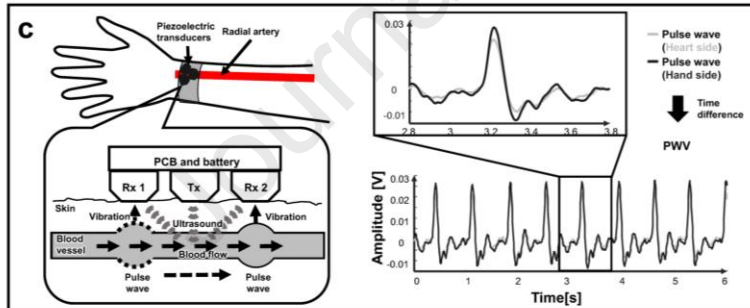
Piezoelectric thin film sensor based on elastomer



Pulse wave piezoelectric sensor



Multimodal cardiovascular information monitor



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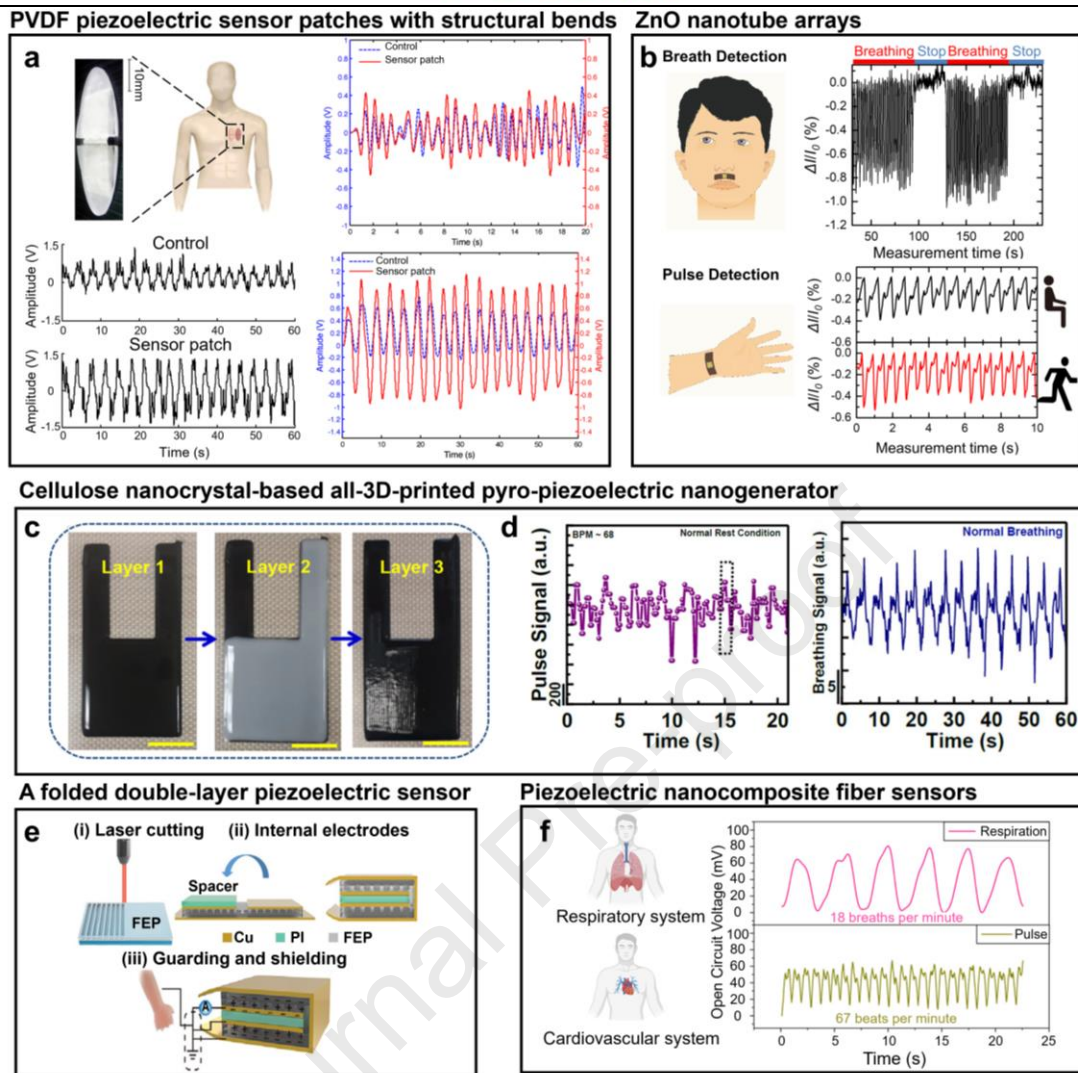
Fig. 7. Piezoelectric sensors for BP and vascular assessment via dual-site PWV measurement. (a) Wireless wristband system integrating folded piezoelectric sensors for continuous BP monitoring and local PWV estimation. Reproduced with permission [121]. Copyright 2023, Springer Nature. (b) Structural diagram and working principle of a PVDF-based sensor fabricated on an elastomeric substrate. Reproduced with permission [125]. Copyright 2024, American Chemical Society. (c) Multimodal monitoring platform integrating piezoelectric, ultrasound, and vibrational sensing for bilateral pulse wave acquisition and PWV extraction. Reproduced with permission [126]. Copyright 2018, Springer Nature. (d) Pulse wave velocity measurement using dual piezoelectric sensors placed along the radial artery. (e) PWV values in patients with premature atrial and ventricular contractions (PACs and PVCs), compared to healthy individuals. Reproduced with permission [129]. Copyright 2021, MDPI.

572 3.3 Cardiopulmonary monitoring via multiparametric piezoelectric sensing

573 Recent advances in flexible piezoelectric sensors have supported multiparameter
574 monitoring of heart rate variability (HRV) and the RR interval, combining simultaneous
575 signal acquisition with data fusion to improve diagnostic value [133-135]. These studies
576 emphasize the technical advantages of flexible piezoelectric sensors, including high
577 sensitivity, real-time performance, and environmental friendliness. As early as 2007,
578 Bu et al. [136] proposed a non-contact cardiopulmonary signal monitoring system for
579 sleep, based on a flexible AlN piezoelectric thin-film sensor. This sensor can detect
580 subtle pressure variations on the human back, induced by respiration and heartbeat;
581 when these are combined with empirical mode decomposition (EMD) algorithms, the
582 sensor effectively extracts and separates respiratory and cardiac signals. In the post-
583 COVID-19 era, a high-sensitivity piezoelectric sensor based on PZT has been
584 developed for the simultaneous monitoring and fusion of heart sounds and pulmonary
585 signals, enabling noninvasive cardiopulmonary function assessment in both healthy
586 individuals and discharged pneumonia patients [137]. Wang et al. [138] developed a
587 wearable piezoelectric patch that enables real-time, noninvasive monitoring of
588 cardiopulmonary coupling by synchronously capturing respiration and heartbeat signals.

589 To solve problems such as poor flexibility and signal stability, Chiu et al. [139]
590 developed a piezoelectric patch sensor based on a curved PVDF structure, achieving a
591 151% increase in respiratory signal detection efficiency due to the curved design (**Fig.**
592 **8a**). This sensor captures heartbeat and respiratory signals with high precision by
593 detecting periodic chest wall deformations and pulsatile vibrations, providing real-time

594 synchronous monitoring. This innovation supports early detection of cardiopulmonary
595 health anomalies. Flexible piezoelectric devices based on 1D inorganic nanomaterials
596 have demonstrated excellent performance. It has been shown that high-quality ZnO
597 nanostructures can be grown on graphene films without catalysts [140]. Park et al. [141]
598 fabricated highly sensitive, flexible pressure sensors by growing ZnO nanotube arrays
599 with controlled positions and dimensions on graphene substrates (**Fig. 8b**). These
600 sensors exhibit high sensitivity (-4.4 kPa^{-1}), enabling accurate monitoring of
601 respiratory and pulse signals and demonstrating utility in the early diagnosis of
602 pulmonary and cardiovascular diseases. The performance of ZnO nanotubes is
603 attributed to their high aspect ratio and ultra-thin wall structure. In recent studies, Maity
604 et al. [142] proposed a fully 3D-printed pyroelectric–piezoelectric nanogenerator (Py-
605 PNG) based on cellulose nanocrystals (CNC) (**Fig. 8c**). This system simultaneously
606 harvests mechanical and thermal energy, functioning as an electronic skin sensor for
607 the early detection of cardiopulmonary dysfunctions. Such integrated sensors open new
608 possibilities for portable monitoring devices and personalized healthcare applications
609 (**Fig. 8d**). Continuous monitoring of arterial pulse via epidermal pressure sensors is
610 crucial for the early detection of cardiovascular disease and personal health assessment.
611 Comparatively, Han et al. [143] utilized a foldable dual-layer piezoelectric sensor to
612 expand monitoring capabilities, capturing not only heartbeats and respiratory sounds
613 but also Korotkoff sounds (**Fig. 8e**). These innovations indicate that flexible
614 multifunctional sensors are becoming a critical development area for cardiovascular
615 health monitoring technologies.



616

617

618 **Fig. 8.** Piezoelectric sensors for cardiopulmonary signal monitoring. (a) PVDF sensor

619 patches with structural bending for simultaneous respiration and pulse detection on the

620 chest wall. Reproduced with permission [139]. Copyright 2013, Elsevier. (b) ZnO

621 nanotube pressure sensors for monitoring breathing cycles and pulse dynamics under

622 motion and apnea conditions. Reproduced with permission [141]. Copyright 2021,

623 Springer Nature. (c) Layer-by-layer fabrication of an all-3D-printed cellulose

624 nanocrystal pyro-piezoelectric nanogenerator. (d) Output signals corresponding to

625 normal and rapid breathing states captured by the device in (c). Reproduced with

626 permission [142]. Copyright 2023, American Chemical Society. (e) Schematic of a

627 folded double-layer piezoelectric sensor system with internal shielding and multilayer

628 electrode configuration. Reproduced with permission [143]. Copyright 2023, WILEY-

629 VCH. (f) Nanocomposite fiber-based piezoelectric sensor for real-time monitoring of

630 respiratory and pulse signals. Reproduced with permission [144]. Copyright 2024,

631 American Chemical Society.

632 MoS₂ has been widely reported to enhance the performance of PVDF-based

633 piezoelectric nanogenerator (PENG) [145, 146]. Hasan et al. [144] developed a wireless

634 piezoelectric sensor by embedding MoS₂ into PVDF-based fibers. Enhanced interfacial
635 polarization significantly improved the electromechanical conversion efficiency,
636 enabling precise cardiovascular signal prediction when integrated with ML algorithms
637 (**Fig. 8f**). Integrating AI with flexible sensors has also emerged as a research focus to
638 improve data processing accuracy and efficiency. Ahmad et al. [147] proposed an
639 innovative wearable system that enables real-time coupling analysis of HR and RR,
640 offering novel solutions for personalized health management. These advances highlight
641 the transition of HRV and RR-based monitoring technologies from single-function
642 detection to complex multi-parameter analysis, paving the way for future health
643 monitoring and management applications.

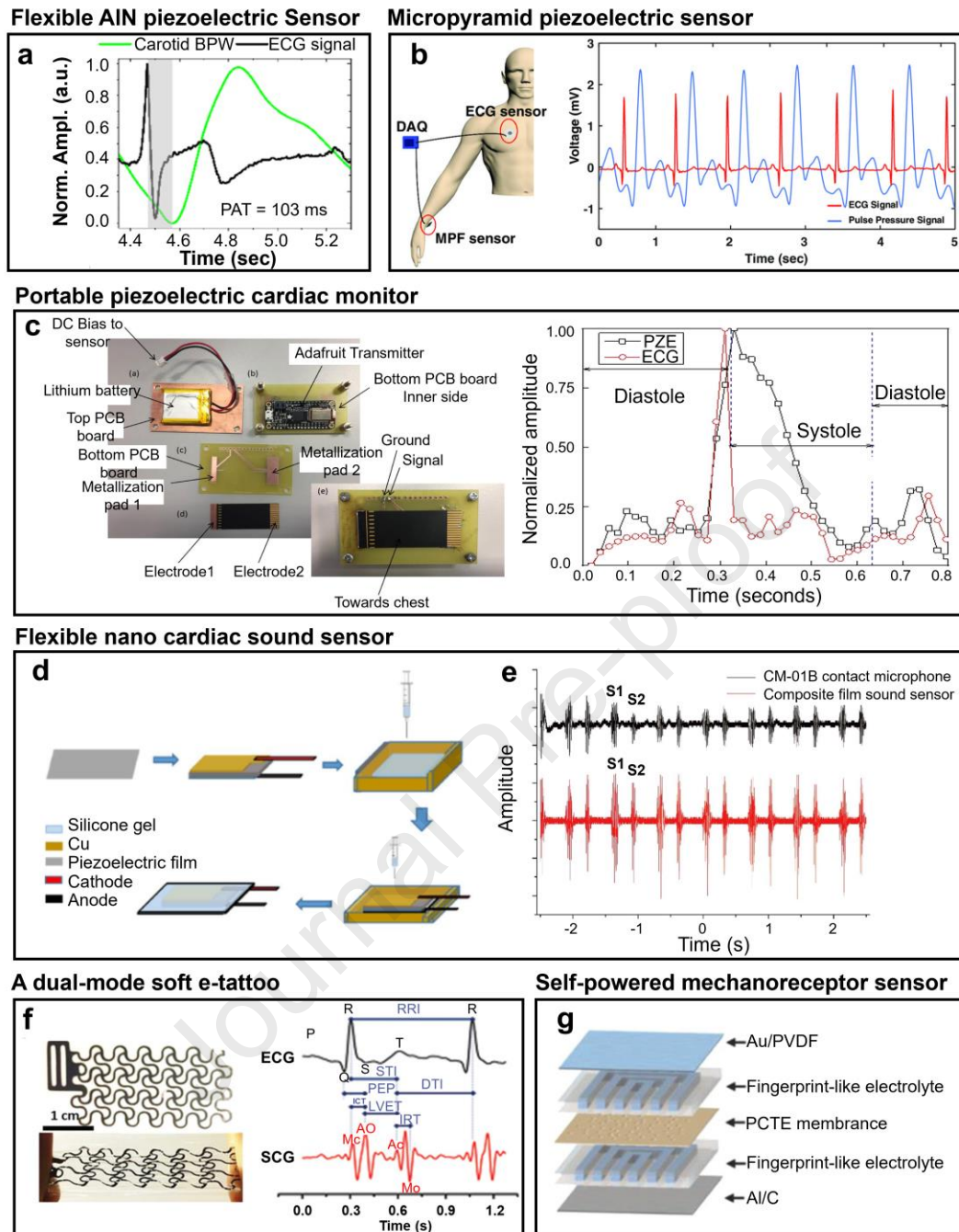
644 Several advanced devices utilizing piezoelectric sensors are already commercially
645 available. EarlySense (an Israeli medical device company) has developed an under-
646 mattress system that detects mechanical vibrations from cardiac and respiratory activity,
647 transmitting real-time data for centralized monitoring and alerting. Clinical studies by
648 Harvard Medical School involving 7,643 patients have shown that this system
649 significantly reduces hospital stays, emergency interventions, and postoperative ICU
650 durations [148]. Similarly, companies like Sensiotec in the U.S. and Emfit in Europe
651 have developed comparable non-contact sensor solutions. The Emfit QS system is the
652 world's first non-contact sleep monitoring device with HRV monitoring functionality
653 [149, 150]. These products provide new possibilities for noninvasive monitoring
654 technologies in healthcare, demonstrating broad prospects for clinical applications.

655 **3.4 Cardiac function evaluation through multimodal fusion**

656 Cardiac function monitoring plays a critical role in the prevention, diagnosis, and
657 management of cardiovascular diseases. While ECG remains the clinical gold standard
658 for assessing cardiac electrical activity [151, 152], increasing attention has been
659 directed toward integrating complementary sensing modalities to achieve more
660 comprehensive cardiac evaluation. Piezoelectric sensing technology offers a highly
661 sensitive and portable alternative for ECG monitoring. By leveraging the direct
662 piezoelectric effect, these sensors can non-invasively capture mechanical signals
663 associated with cardiac activity—such as micro-vibrations or thoracic deformations—
664 which are temporally correlated with electrocardiographic events, thereby enabling
665 indirect assessment or fusion with ECG signals [153].

666 Recent studies have demonstrated the effectiveness of integrating piezoelectric
667 sensors with ECG signals for multimodal cardiac monitoring. Cinquino et al. [154]
668 developed a flexible, biocompatible AlN piezoelectric sensor capable of recording
669 pressure waveforms from multiple arterial sites. By synchronizing these piezoelectric
670 signals with ECG, they extracted various cardiovascular indicators—including PWV,
671 SI, and cardio-ankle vascular index (CAVI)—to assess both central and peripheral
672 arterial stiffness (**Fig. 9a**). Similarly, Kim et al. [155] designed a self-powered wearable
673 piezoelectric sensor with micropyramid structures, which combined pulse signals and
674 ECG to estimate PTT and PWV, enabling accurate systolic blood pressure (SBP)
675 monitoring (**Fig. 9b**). These works highlight the potential of multimodal piezoelectric
676 sensing systems for accurate, noninvasive, and continuous cardiac function monitoring
677 in wearable applications.

678 Moreover, Mokhtari et al. [156] developed a lightweight, Bluetooth-based
679 piezoelectric system for real-time heart monitoring. By aligning piezoelectric signals
680 with ECG data, they extracted key cardiac parameters and used cross-correlation to
681 detect abnormalities (**Fig. 9c**). This method enables accurate, low-power monitoring
682 and classification of cardiac events. Luo et al. [157] developed a flexible nano-cardiac
683 sensor based on a P(VDF-TrFE)/KNN/GR composite film (**Fig. 9d**), significantly
684 improving sensitivity and accuracy in cardiac disease diagnosis. By leveraging the high
685 dielectric constant of KNN, the high conductivity of graphene, and the excellent
686 piezoelectric properties of P(VDF-TrFE), the sensor successfully captures weak heart
687 sound signals. When combined with the RepMLP classification model, the sensor's
688 high sensitivity complements the model's precise classification capabilities, facilitating
689 heartbeat collection and real-time automatic diagnosis and offering new possibilities
690 for early clinical monitoring (**Fig. 9e**).



691

692

693 **Fig. 9.** Multimodal piezoelectric sensors for integrated cardiac function assessment. (a)

694 Simultaneous measurement of carotid pulse pressure and ECG signals for PWV

695 estimation using a flexible AlN-based piezoelectric sensor. Reproduced with

696 permission [154]. Copyright 2025, Elsevier. (b) Concurrent acquisition of pulse and

697 ECG waveforms using a micropyramid-structured piezoelectric sensor. Reproduced

698 with permission [155]. Copyright 2022, WILEY-VCH. (c) Portable cardiac monitoring

699 system integrating piezoelectric sensing, signal acquisition, and wireless transmission,

700 with synchronized ECG and piezoelectric cycle comparison. Reproduced with

701 permission [156]. Copyright 2019, Elsevier. (d–e) Design and performance of a flexible

702 nanocomposite cardiac sound sensor, showing the fabrication process and heart sound

signals compared with a standard contact microphone. Reproduced with permission

703 [157]. Copyright 2023, IOP Publishing. (f) Dual-mode soft e-tattoo platform enabling
704 simultaneous detection of ECG and seismocardiography (SCG), with annotated cardiac
705 time intervals. Reproduced with permission [65]. Copyright 2019, WILEY-VCH. (g)
706 Schematic of a self-powered mechanoreceptor sensor with a fingerprint-mimicking
707 multilayer structure. Reproduced with permission [158]. Copyright 2018, WILEY-
708 VCH.

709

710 More and more researchers are developing PVDF-based stretchable
711 electromechanical sensors based on micropatterned PVDF membrane [159], ribbon-
712 like PVDF embedded in Ecoflex [160], and PVDF islands interconnected by serpentine
713 metal wires [161] on PVDF-based stretchable electromechanical sensors. Ha et al. [65]
714 developed a soft, stretchable e-tattoo that integrates piezoelectric and ECG sensors for
715 synchronous recording of SCG and ECG signals (**Fig. 9f**). This fusion enables the
716 extraction of detailed cardiac time intervals, such as the systolic time interval (STI),
717 which shows a strong negative correlation with BP. By aligning mechanical and
718 electrical signals on a single skin-conformal device, the study demonstrates a low-
719 profile, wearable solution for continuous, noninvasive cardiovascular monitoring. Chun
720 et al. [158] developed a self-powered mechanoreceptor-inspired sensor that mimics the
721 fast- and slow-adapting responses of human skin by combining a piezoelectric PVDF
722 film with an ion-channel-based layer (**Fig. 9g**). Instead of pursuing fusion with ECG
723 signals, like previous studies, this work achieves signal integration at the material level,
724 using the piezoelectric layer to detect dynamic pulses and the ionic component for static
725 pressure. This dual-mode sensing enables real-time monitoring of pulse waves, BCG,
726 and tactile stimuli, offering a bioinspired, low-power approach to cardiovascular and
727 sensory signal tracking.

728 In addition to electro-mechanical fusion, recent efforts have explored the
729 integration of piezoelectric sensors with optical signals, particularly PPG, to enable
730 complementary cardiovascular assessment. Jin et al. [162] developed a flexible
731 optoacoustic platform that couples PVDF-based piezoelectric receivers with microlens
732 arrays, allowing multiparametric evaluation of vascular dynamics, blood oxygenation,
733 and endothelial function through light-induced acoustic signals. Deng et al. [163]
734 introduced a fully wearable tonometric system combining piezoelectric pressure arrays
735 with optical sensors and adaptive mechanical control for real-time, medical-grade
736 hemodynamic monitoring. Samartkit et al. [164] further demonstrated that combining
737 PZT sensors with PPG enables pulse transit time estimation through a modified
738 algorithm, supporting accurate, low-power BP tracking in ambulatory settings. These
739 multimodal strategies highlight the central role of piezoelectric sensing in enabling
740 continuous, high-resolution, and integrative cardiac function monitoring across
741 electrical, mechanical, and optical domains.

742 **3.5 Intelligent monitoring systems**

743 **3.5.1 AI-driven signal interpretation**

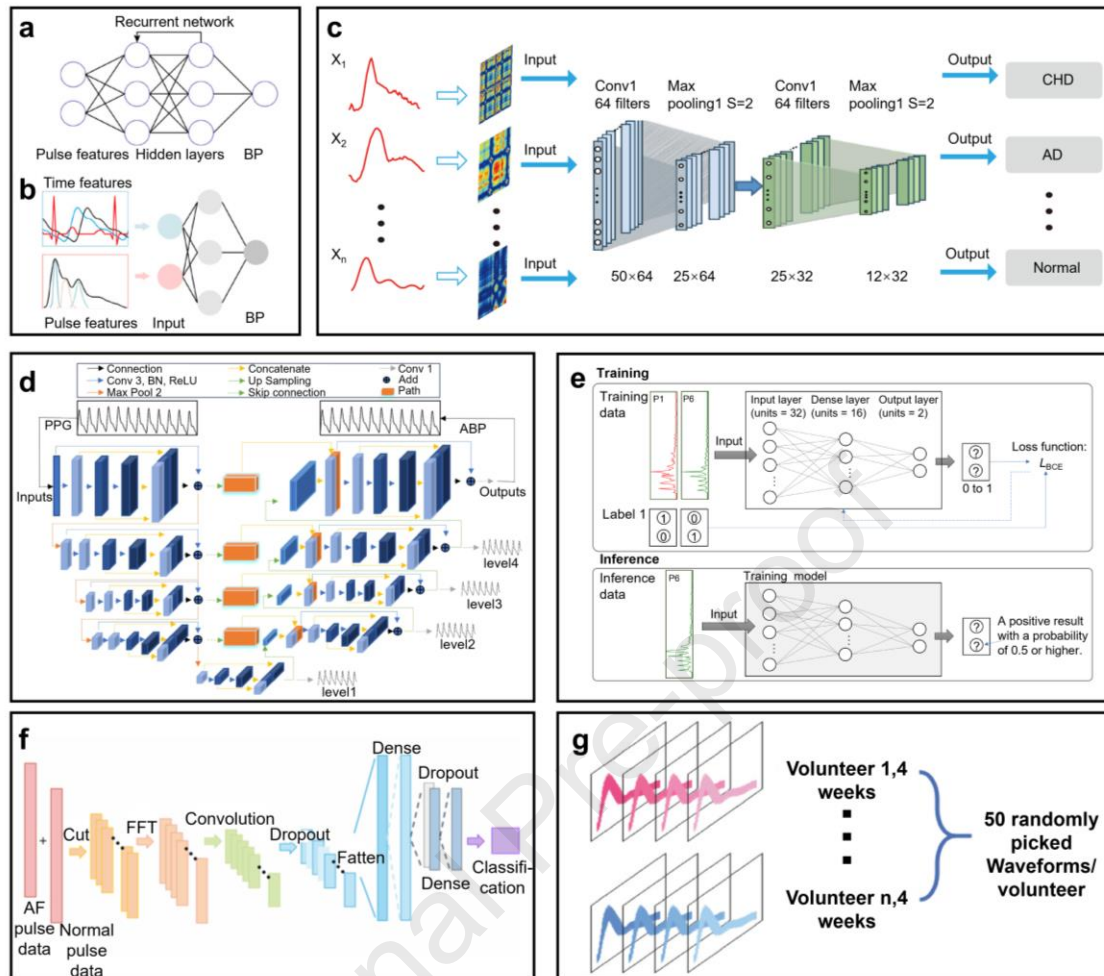
744 The integration of AI has significantly enhanced the performance of
745 cardiovascular monitoring systems by improving data processing accuracy and
746 enabling multimodal analysis [165]. Combined with advanced piezoelectric sensors and
747 DL algorithms, these systems support early disease detection, personalized health
748 management, and continuous noninvasive monitoring, offering broad clinical and daily
749 healthcare applications [166, 167]. Several studies have demonstrated the effectiveness

750 of AI-based approaches. Ahmadpour et al. [168] introduced a piezoelectric
751 metamaterial BP sensor, employing Bayesian optimization and ML regression models
752 to identify optimal design parameters. Wang et al. [169] developed a piezoelectric
753 system for continuous BP estimation based on initial values and pressure accumulation,
754 achieving a mean absolute error under 5 mmHg and a standard deviation below 8
755 mmHg. To address the needs of maternal health monitoring, Nie et al. [170] integrated
756 a piezoelectric thin-film pulse sensor with modal energy ratio (MER) analysis based on
757 EMD. The system successfully analyzed data from 83 pregnant participants, enabling
758 early identification of health risks and pregnancy-related indicators.

759 Accurately tracking arterial mechanical properties, which vary significantly
760 between individuals and can change over time due to external stimuli, poses a
761 formidable challenge for understanding their impact on BP fluctuations. Recurrent
762 neural networks (RNNs) effectively account for the dynamic variability of arterial
763 characteristics, thereby enhancing the stability of long-term models (**Fig. 10a**).
764 Additionally, combining pulse features with propagation characteristics, such as PAT
765 and PTT, further improves model accuracy and long-term reliability [171] (**Fig. 10b**).
766 Sun et al. [172] developed an intelligent cardiovascular disease diagnosis system
767 integrating a 2D Bi₂O₂Se PENG with DL technology. This system combines self-
768 powered pulse sensors with DL models to accurately identify nine common
769 cardiovascular diseases (**Fig. 10c**). Huang et al. [173] developed a BP monitoring
770 system based on a flexible piezoelectric sensor made from PVDF and MXene
771 composites. The sensor is integrated with a DL model (MLSU-net) that predicts BP

772 waveforms using PPG signals, incorporating multi-scale convolutional kernels and long
773 short-term memory (LSTM) networks. This system enables real-time BP estimation
774 using a single-channel signal, overcoming data filtering issues and improving
775 prediction accuracy (**Fig. 10d**). Karin et al. [174] demonstrated a customized sensor
776 integrated into a chair, enabling non-contact monitoring where arterial vibrations
777 modulate pressure applied to the sensor. A deep neural network model exhibited
778 significant potential for personalized identification of abnormal biosignals in
779 individuals (**Fig. 10e**).

780 Cao et al. [175] developed an intelligent atrial fibrillation (AF) recognition system
781 that integrates AI with the traditional Chinese medicine (TCM) concept of pulse
782 diagnosis. A wearable, flexible three-dimensional pressure sensor array was employed
783 to collect pulse signals from the Cun, Guan, and Chi positions, which were then
784 analyzed using a convolutional neural network (CNN) to accurately distinguish
785 between healthy and AF pulse patterns, achieving a recognition accuracy of 93.2% (**Fig.**
786 **10f**). Similarly, Chu et al. [176] designed an aortic pulse sensing system based on a
787 sandwich-structured piezoelectric material (FEP/Ecoflex/FEP). By leveraging ML-
788 based big data analysis, the system enabled precise identification and classification of
789 individual pulse waveforms (**Fig. 10g**). This sensing platform allows for continuous HR
790 monitoring, arrhythmia detection, and BP estimation, offering a high-precision,
791 noninvasive, AI-assisted solution for cardiovascular health monitoring in mobile
792 healthcare settings.



793

794 **Fig. 10.** AI-enabled analysis of piezoelectric pulse signals for cardiovascular health
 795 monitoring. (a) RNN model for extracting temporal features from pulse signals to
 796 estimate BP. (b) Multifactor model integrating time-domain and morphological features
 797 for enhanced BP prediction. Reproduced with permission [171]. Copyright 2024,
 798 American Chemical Society. (c) CNN-based classification of cardiovascular disease status
 799 using piezoelectric pulse data. Reproduced with permission [172]. Copyright
 800 2024, Elsevier. (d) Architecture of a multi-level supervised network mapping PPG to
 801 arterial blood pressure (ABP). Reproduced with permission [173]. Copyright 2025,
 802 Elsevier. (e) Workflow of model training and inference using pulse waveform data.
 803 Reproduced with permission [174]. Copyright 2024, MDPI. (f) CNN framework for
 804 arrhythmia classification based on pulse waveform transformation and feature
 805 extraction. Reproduced with permission [175]. Copyright 2025, American Chemical
 806 Society. (g) Schematic of the pulse pattern clustering process across volunteers for
 807 waveform discrimination and population-based analysis. Reproduced with permission
 808 [176]. Copyright 2018, WILEY-VCH.

809

810 3.5.2 IoT-enabled remote connectivity

811 The IoT has emerged as a transformative force in digital healthcare, supporting

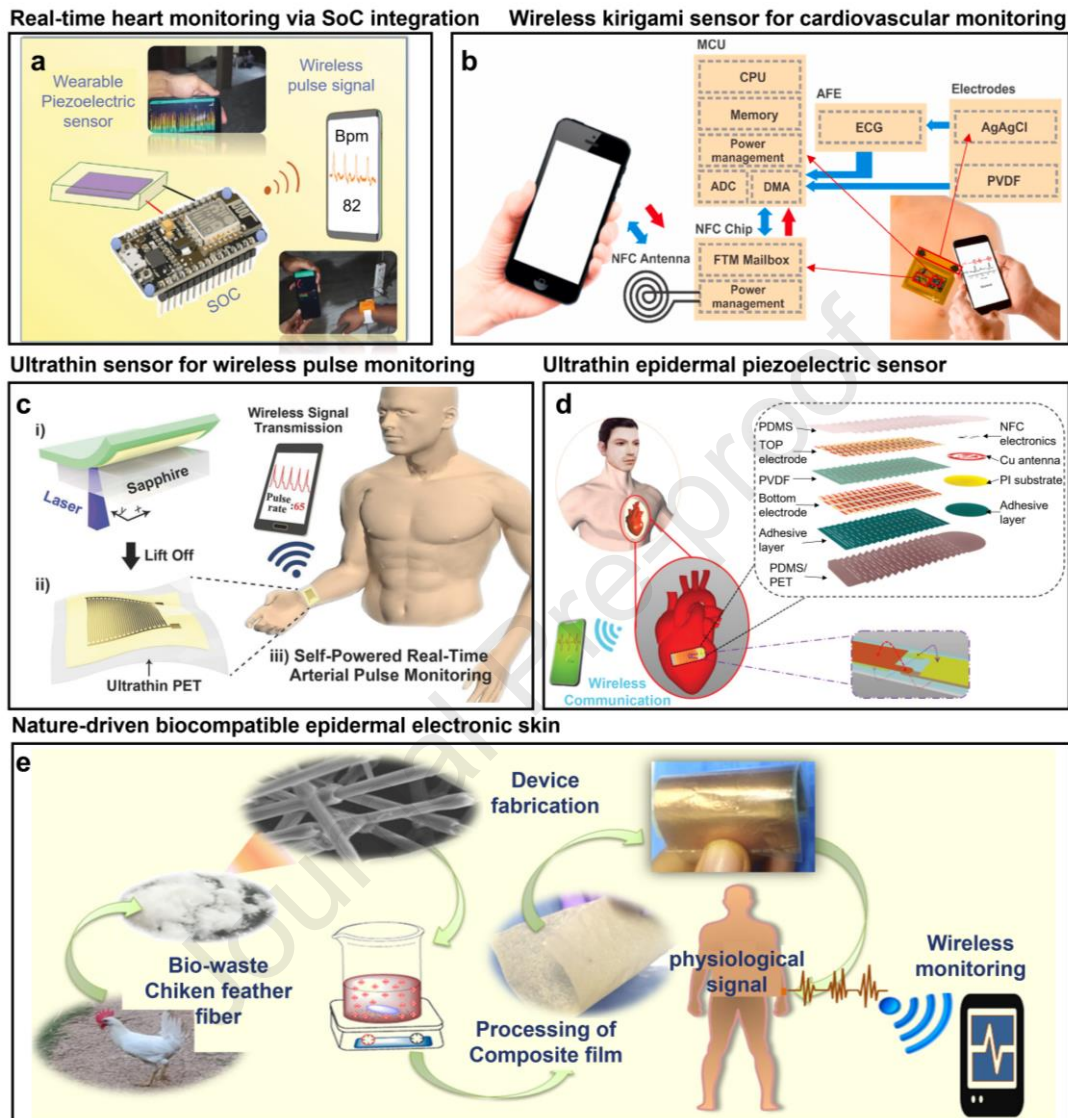
812 continuous, real-time, and remote monitoring of physiological parameters. Typically
813 composed of four components—smart sensors, cloud computing, wireless networks,
814 and analytical software [177]—IoT-enabled cardiovascular systems rely on wireless
815 technologies such as Bluetooth Low Energy (BLE), Wi-Fi, Near-field communication
816 (NFC), and cellular networks to transmit physiological data from sensors to mobile or
817 cloud-based platforms for further analysis and clinical decision-making. Babu et al.
818 [178] developed a highly sensitive flexible piezoelectric sensor for arterial pulse wave
819 recording and cardiovascular health assessment (**Fig. 11a**). The system integrated a
820 system-on-chip (SoC) for wireless data transmission, enabling real-time pulse signal
821 delivery to remote devices and facilitating early prediction of cardiovascular
822 abnormalities with an accuracy exceeding 94%. In another example, Hesar et al. [179]
823 engineered a flexible, battery-free epidermal electronic system (EES) with integrated
824 ECG and SCG sensors to simultaneously acquire electrical and mechanical cardiac
825 signals (**Fig. 11b**). This system utilized NFC technology for wireless power and data
826 transfer, combined with automatic signal analysis and health state recognition, and
827 successfully identified cases of cardiopulmonary hypertension.

828 Park et al. [63] developed a self-feeding flexible piezoelectric pulse sensor based
829 on an ultrathin PZT film, capable of conformally adhering to human skin for high-
830 sensitivity, real-time monitoring of radial and carotid pulse waves (**Fig. 11c**). The sensor
831 system incorporated a microcontroller unit (MCU) and BLE module to wirelessly
832 transmit data to smartphones, while also supporting real-time feedback via integrated
833 LEDs and acoustic alerts. Similarly, a kirigami-inspired flexible piezoelectric sensor

834 system was developed by Sun et al. [180], featuring excellent skin conformity and
835 energy autonomy. The system, equipped with an NFC module, enabled stable, battery-
836 free wireless data transmission, providing a compact and low-power IoT solution for
837 wearable and implantable cardiovascular monitoring (**Fig. 11d**). Kar et al. [181]
838 developed a novel composite piezoelectric material by repurposing chicken feathers
839 into processable chicken feather fibers (CFF) and incorporating them as fillers into
840 PVDF (**Fig. 11e**). The device enabled remote real-time monitoring via Wi-Fi
841 connectivity and was used for monitoring various physiological signals, including body
842 motion, throat activity, and pulse rate, exhibiting excellent sensitivity and offering
843 broad application in telemedicine and personalized health management.

844 Existing studies have evaluated the effectiveness of ex vivo sensors in predicting
845 and detecting a wide range of cardiac events. Yu et al. [182] developed a non-contact
846 BCG monitoring system based on piezoelectric ceramics, which was clinically
847 validated overnight in 37 hospitalized patients with sleep apnea syndrome (SAS). The
848 system integrated AI algorithms and embedded data transmission modules, confirming
849 its feasibility for accurate HRV analysis in clinical settings. Lin et al. [183] further
850 proposed a BLE-enabled, wireless multi-lead polysomnography (PSG) system for sleep
851 monitoring, capable of real-time transmission of multichannel physiological data.
852 Comparative clinical tests with the standard Alice 5 PSG system showed a high degree
853 of agreement in sleep stage recognition, supporting the feasibility of this IoT-based
854 system for low-power, continuous cardiopulmonary monitoring in home environments.
855 These studies have fueled the emergence of FDA-approved noninvasive cardiac

856 monitoring systems that promise to aid in the diagnosis of multiple HRV-related
 857 syndromes [184].



858

859 **Fig. 11.** IoT-integrated piezoelectric platforms for wireless cardiovascular health
 860 monitoring. (a) Real-time arterial pulse sensing and wireless data transmission using a
 861 piezoelectric sensor integrated with a SoC platform. Reproduced with permission [178].
 862 Copyright 2023, WILEY-VCH. (b) Schematic of an electronic epidermal system (EES)
 863 comprising power, signal processing, and ECG modules with NFC-enabled wireless
 864 communication. Reproduced with permission [179]. Copyright 2023, Elsevier. (c)
 865 Fabrication and application of an ultrathin self-powered piezoelectric sensor for real-
 866 time arterial pulse monitoring, based on transferred PZT films on PET substrates.
 867 Reproduced with permission [63]. Copyright 2017, WILEY-VCH. (d) Integrated
 868 multilayer piezoelectric sensor and wireless patch for epidermal cardiovascular
 869 monitoring, with details of component architecture and electrode patterning.
 870 Reproduced with permission [180]. Copyright 2019, WILEY-VCH. (e) Development

871 of a nature-derived organohydrogel-based epidermal electronic skin from chicken
872 feather waste, enabling biocompatible signal acquisition and smartphone-based
873 wireless monitoring. Reproduced with permission [181]. Copyright 2019, American
874 Chemical Society.

875

876 **3.6 Comparative evaluation of sensing technologies**

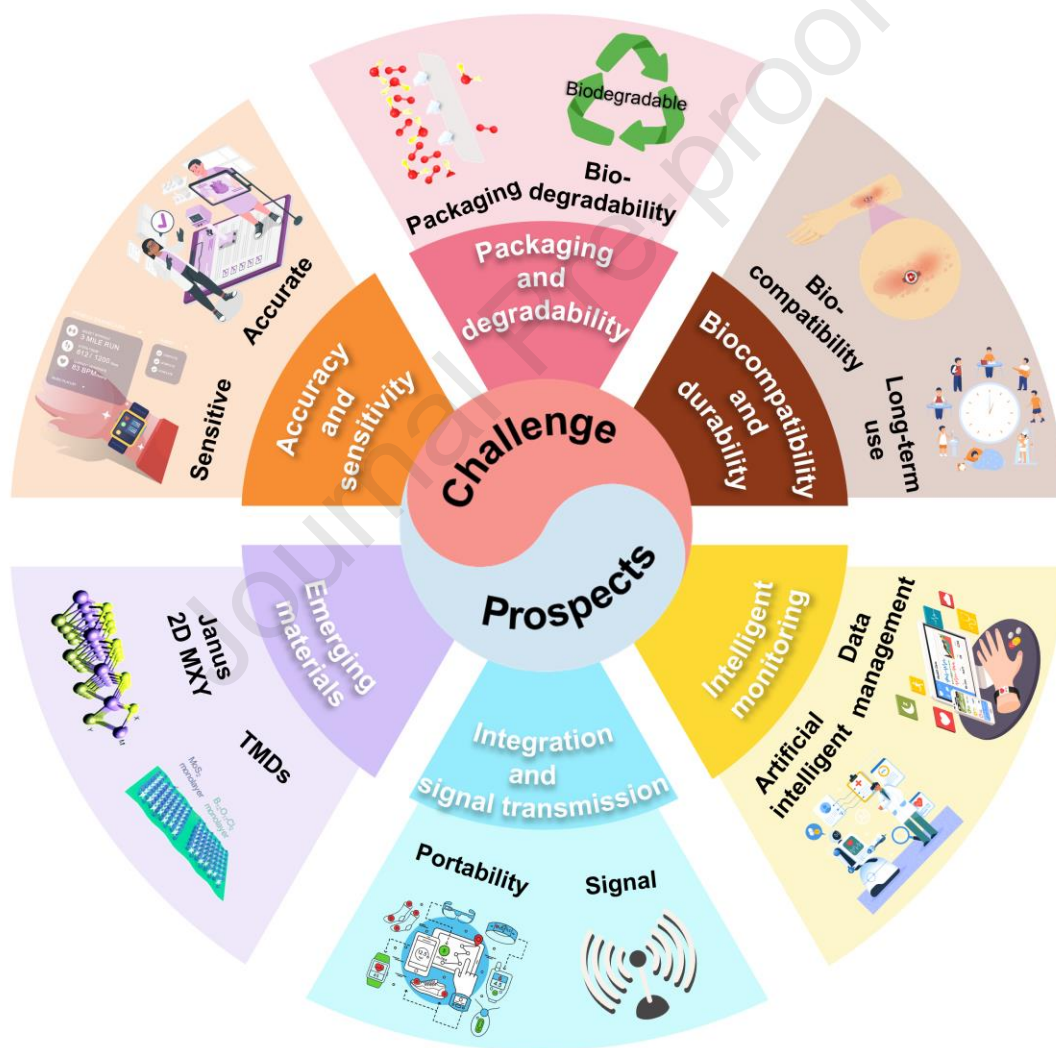
877 Although piezoelectric technology offers numerous advantages in cardiovascular
878 health monitoring, including high sensitivity, the absence of external power
879 requirements, and exceptional flexibility, it also has certain limitations. For instance,
880 some sensors exhibit relatively slow response times or insufficient stability under long-
881 term cyclic loading, which may limit their effectiveness in continuous monitoring
882 applications. These challenges are often caused by variations in the choice of sensitive
883 materials and structural designs, resulting in significant differences in sensing
884 performance. As summarized in **Table 3**, a variety of flexible piezoelectric sensors have
885 been developed for cardiovascular health monitoring, addressing parameters such as
886 arterial health, cuffless blood pressure, and multiparametric cardiopulmonary signals.
887 These sensors exhibit substantial variability in sensitivity, response time, and
888 operational stability, depending on the materials, structural configurations, and sensing
889 mechanisms employed.

890 Overall, piezoelectric technology is rapidly advancing in the field of
891 cardiovascular health monitoring, providing an effective means to enhance the
892 prevention, diagnosis, and treatment of cardiovascular diseases. With further research
893 and technological progress, the development of more efficient and accurate
894 piezoelectric monitoring devices is anticipated, promising revolutionary improvements
895 in cardiovascular health management.

896 **4 Challenges and outlook**897 **4.1 Technical and clinical challenges**

898 Although piezoelectric technology exhibits tremendous potential in cardiovascular
 899 health monitoring, it also faces a range of challenges. Below is a detailed discussion of
 900 these challenges and corresponding strategies to address them (**Fig. 12**).

901



902

903 **Fig. 12.** Challenges and outlook for piezoelectric technologies in cardiovascular health
 904 monitoring. This figure outlines the primary challenges, such as packaging and
 905 degradability, biocompatibility, long-term stability, sensitivity, and accuracy, alongside
 906 promising prospects, including material innovation, signal acquisition, wireless
 907 transmission, device miniaturization, and AI integration. Emerging directions feature

908 the use of Janus materials, transition-metal dichalcogenides (TMDs), conformal device
909 integration, and AI-driven data analysis for personalized cardiovascular health
910 management. Reproduced with permission [185]. Copyright 2023, WILEY-VCH.
911 Reproduced with permission [186]. Copyright 2020, ROYAL SOCIETY OF
912 CHEMISTRY.

913

914 (1) Monitoring accuracy and sensitivity

915 Achieving high accuracy and sensitivity remains a critical challenge for
916 piezoelectric sensors in cardiovascular monitoring, where subtle physiological changes
917 often carry significant clinical value. However, signal quality can be compromised by
918 environmental noise, electromagnetic interference, and limitations in material or
919 structural design. Recent advances in materials science, such as PVDF composites with
920 carbon nanotubes or conductive polymers, have enhanced signal transduction,
921 flexibility, and biocompatibility [187-191]. Multilayer structures and nanocomposites
922 further amplify weak bio-signals by increasing effective piezoelectric output and
923 optimizing stress distribution. Representative efforts include folded-structure electret
924 sensors for low-frequency non-contact sensing [192] and ML algorithms-assisted
925 microstructure optimization to boost material sensitivity and stability [193]. The
926 convergence of materials innovation, structural engineering, and intelligent analytics is
927 essential for overcoming current performance limitations and advancing toward reliable,
928 high-precision, and multifunctional piezoelectric health monitoring systems.

929 (2) Packaging and biodegradability

930 For implantable piezoelectric devices, ensuring both long-term stability and
931 biological safety requires careful consideration of material biodegradability and
932 packaging strategies. Biodegradable piezoelectric materials, often derived from natural

933 polymers or bioresorbable composites, can safely degrade after completing their
934 monitoring tasks, reducing chronic tissue responses and postoperative complications
935 [194-199]. However, their mechanical and electrical performance may be inferior to
936 non-degradable counterparts, necessitating structural optimization and surface
937 modifications to enhance durability and compatibility [200-202]. Meanwhile,
938 packaging is essential for isolating sensors from biological fluids and maintaining
939 functional integrity. Flexible polymers such as PDMS and PLGA are widely used due
940 to their biocompatibility and barrier properties [203, 204]. Advanced transient systems
941 combine biodegradable substrates with multilayer encapsulants—such as waxes or
942 polyanhydrides—to tune operational lifespan from hours to weeks, depending on the
943 clinical need [205-207]. These co-engineered approaches to material degradation and
944 protective encapsulation are crucial for enabling safe, effective, and temporally
945 controlled operation of next-generation implantable piezoelectric sensors.

946 (3) Biocompatibility and durability

947 Ensuring biocompatibility and durability is fundamental to the long-term
948 functionality of piezoelectric sensors in physiological environments. Poor material
949 compatibility can trigger immune responses or inflammation, while insufficient
950 durability — due to mechanical fatigue, chemical corrosion, or environmental
951 degradation—may lead to signal instability, especially in flexible devices under
952 repeated deformation. Traditional materials like PZT and BaTiO₃ often present toxicity
953 risks, whereas biocompatible alternatives such as PVDF and ZnO offer safer
954 interactions with tissue and are now widely adopted in implantable systems [208-211].

955 To further improve biological integration, surface engineering techniques and
956 biodegradable materials have been employed, minimizing adverse immune responses
957 and reducing post-implantation complications [212-215]. Simultaneously, durability is
958 reinforced through the use of high-strength composites, flexible nanocomposites, and
959 protective barrier coatings—such as polymer or ceramic encapsulants—which enhance
960 resistance to mechanical and chemical stress [216-218]. These material and structural
961 strategies collectively improve the safety, stability, and lifespan of piezoelectric devices,
962 supporting their reliable operation in complex and dynamic in vivo conditions.

963 (4) Data processing and privacy protection

964 Cardiovascular monitoring generates large volumes of data requiring real-time
965 processing, high accuracy, and robust privacy safeguards. Cloud and edge computing
966 architectures help address these needs: cloud platforms support large-scale analysis,
967 while edge computing reduces latency by enabling local signal processing [219-222].
968 Emerging frameworks combining blockchain and federated learning enable
969 decentralized cardiovascular data analysis while preserving data ownership and
970 integrity [223]. ML methods, including support vector machines and deep neural
971 networks, enhance feature extraction and anomaly detection [224, 225]. To secure
972 sensitive health data, encryption protocols, differential privacy, and blockchain-based
973 access control have been widely adopted [226]. These technologies help prevent
974 unauthorized access and foster trust in wearable and implantable piezoelectric
975 monitoring systems.

976 **4.2 Outlook and conclusion**

977 Piezoelectric technology is transforming cardiovascular health monitoring by
978 offering high sensitivity, rapid response, and inherent self-powered functionality. These
979 attributes enable the real-time detection of subtle biomechanical signals such as arterial
980 pulsations, cardiac microvibrations, and BP variations, supporting continuous,
981 noninvasive, and high-fidelity monitoring across both wearable and implantable
982 formats. The ability to operate without external power sources also facilitates long-term
983 and sustainable physiological tracking.

984 To achieve clinical translation, several challenges must be addressed. The
985 development of lead-free, biodegradable, and intrinsically flexible piezoelectric
986 materials is essential to ensure both biocompatibility and safety, particularly in
987 implantable settings. At the same time, device encapsulation plays a critical role. For
988 biodegradable systems, packaging materials must preserve signal fidelity and
989 mechanical integrity while exhibiting predictable and bio-safe degradation behavior. In
990 addition, the design of the device–tissue interface must support stable performance and
991 intimate contact under dynamically changing physiological conditions.

992 Reliable wireless data transmission is another key requirement. For implantable
993 systems, wired communication is neither practical nor clinically feasible. Therefore,
994 compact and efficient wireless communication modules such as Bluetooth, near-field
995 communication, or radiofrequency backscatter-based systems are necessary to enable
996 real-time physiological monitoring. Passive wireless platforms based on
997 radiofrequency mechanisms are particularly promising. For instance, chipless
998 electronic skins incorporating surface acoustic wave sensors made from ultrathin

999 gallium nitride membranes have demonstrated high-sensitivity, battery-free monitoring
1000 of physiological parameters, including strain, ultraviolet exposure, and pulse. These
1001 technologies offer a viable pathway toward minimally invasive, long-term wearable
1002 and implantable monitoring platforms.

1003 Piezoelectric systems also enable multidimensional cardiovascular monitoring
1004 through two complementary modalities. The first involves the integration of diverse
1005 mechanical signals, including pulse waveforms, heart sounds, cardiac microvibrations,
1006 and arterial pressure changes, into a single sensing unit, providing comprehensive
1007 assessments of cardiac function. The second modality leverages the high sensitivity of
1008 surface acoustic wave sensors to changes in mechanical, chemical, and optical
1009 environments, allowing for the detection of ionic concentrations, biochemical reactions,
1010 and light-triggered responses. Together, these approaches facilitate the development of
1011 compact and integrated systems capable of delivering high-resolution and personalized
1012 cardiovascular diagnostics.

1013 The incorporation of AI and edge computing further extends the potential of
1014 piezoelectric sensing systems. These technologies enable real-time anomaly detection,
1015 continuous risk assessment, and automated clinical decision-making. Concurrently, the
1016 integration of IoT infrastructure supports remote monitoring and decentralized
1017 healthcare delivery, expanding access to continuous cardiovascular diagnostics. Among
1018 the emerging innovations, bioresorbable piezoelectric devices are particularly
1019 promising for postoperative monitoring and use in high-risk patient populations. These
1020 temporary devices provide short-term functionality and degrade safely in vivo,

1021 eliminating the need for surgical retrieval.

1022 In summary, piezoelectric technology is positioned to become a foundational
1023 component of next-generation cardiovascular diagnostic and therapeutic systems.
1024 Continued advances in material development, device encapsulation, wireless
1025 communication, and intelligent data analytics will be essential for realizing clinically
1026 practical, high-performance platforms that seamlessly connect real-time physiological
1027 monitoring with precision medical interventions.

1028

1029 **Competing financial interests**

1030 The authors declare no competing financial interests.

1031

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1038 were sourced from Freepik (<https://www.freepik.com>).

1039

Table 1. Comparative evaluation of cardiovascular monitoring technologies

Technology	Representative materials	Sensitivity	Accuracy	Cost	Ease of use	Power consumption	Applications
Piezoelectric	PVDF, PZT, quartz	$(6.3E^{-7}-10) \text{ V}\cdot\text{Pa}^{-1}$ [73, 227]	98.3% [93]	Cost-effective	Flexible, wearable, high comfort	Self-powered	BP, SCG, Korotkoff sounds, Multimodal monitoring
Piezoresistive	Carbon black, rGO, PEDOT:PSS	$(0.66-284.4) \text{ kPa}^{-1}$ [228, 229]	96.03% [230]	Cost-effective	Flexible, wearable, high comfort	3nW/ Low [230]	HR, RR
Capacitive	PDMS, PU, metal	$(0.148-56.91) \text{ kPa}^{-1}$ [231, 232]	91.2% [233]	Cost-effective	Flexible, wearable, high comfort	7.8 mW/ Mid [234]	HR, RR
PPG	OLED, OPD	$3.5 \times 10^5 \text{ A W}^{-1}$ [13]	99.5% [235]	\$24–210 Medium-cost	Rigid, wearable, moderate comfort	1.66 mW/ Mid [236]	HR, BP, SpO ₂
Traditional ECG	Ag/AgCl	>96%* [237]	>99% [237]	\$288–2302 High-cost	Rigid, non-portable, low comfort	16.4–373.2 mW/ High [238]	ECG, HRV, Arrhythmia classification
Holter	Ag/AgCl	>99%* [239]	> 99% [240]	\$206–4111 High-cost	Rigid, wearable, moderate comfort	>100 mW/ High [241]	Long-term ECG, AF, HRV

1040

* QRS wave recognition rate

1041

Table 2. Advantages and limitations of various piezoelectric materials

Type of material	Advantages	Limitations	Applications
0D material	▲ High surface energy	■ Low mechanical strength	★ Microscale sensors
	▲ Excellent charge coupling	■ Limited structural stability	★ Material optimization
	▲ Easy to integrate into composites	■ Hard to scale	★ Nanogenerators
1D materials	▲ High aspect ratio	■ Difficult manufacturing process	★ Wearable devices
	▲ Strong directional response	■ Lower bulk stability	★ Blood pressure sensors
	▲ Flexible and lightweight	■ Limited long-term durability	★ Implantable monitors
2D materials	▲ Planar structure with anisotropic properties	■ Mechanical durability under cyclic loads	★ Flexible electronics
	▲ Strong piezoelectric effect	■ Limited large-scale integration	★ Cardiac motion monitoring
	▲ Flexible	■ Moderate thermal stability	★ Multi-modal sensors
3D materials	▲ High mechanical stability	■ Rigid and inflexible	★ Ultrasound imaging
	▲ Strong bulk piezoelectricity	■ Relatively heavy	★ Energy harvesting
	▲ Adaptable to complex geometries	■ Requires advanced processing for flexibility	★ Implantable cardiovascular devices

1042

Table 3. Flexible piezoelectric sensors for monitoring CVD-related parameters: materials, principle of operation, and performance

	Mechanism	Sensitive materials	Structure	Sensitivity	Response time	Stability
Arterial health assessment	Piezoelectric	PVDF	Membrane [68]	173 mV/mmHg	30 ms	Number of cycles >50,000
	Piezoelectric	P(VDF-TrFE)	Membrane [73]	0.63 $\mu\text{V}\cdot\text{Pa}^{-1}$	-	Number of cycles >400,000
	Piezoelectric	PVDF/DA	Core-shell structure [86]	-59.4 $\text{pm}\cdot\text{V}^{-1}$	-	Number of cycles >2,000
	Piezoelectric	PVDF	Organohydrogels [242]	1.34 $\text{mV}\cdot\text{kPa}^{-1}$	31 ms	Number of cycles >5,000
	Piezoelectric	BaTiO ₃	Micropyramid balloon catheter [72]	19.12 $\text{mV}\cdot\text{kPa}^{-1}$	-	-
	Piezoelectric	PVDF/HFP	Zigzag-shaped piezoelectric stent [69]	$7.02 \times 10^{-4} \text{V}\cdot\text{Psi}^{-1}$	-	Number of cycles >10,000
	Piezoelectric	PVDF/CFP	Electronic skin [181]	93 $\text{mV}\cdot\text{kPa}^{-1}$	0.88 ms	>7 weeks
	Piezoelectric/Capacitor	GaN	E-skin [66]	10.06 $\text{A}\cdot\text{W}^{-1}$	-	Number of cycles >3,000
Cuffless blood pressure estimation	Piezoelectric	PZT	Piezoelectric thin film [94]	0.062 kPa^{-1}	23 ms	Number of cycles >50,000
	Piezoelectric	PZT	Porous nanocomposite films [96]	9.07 $\text{mV}\cdot\text{kPa}^{-1}$	50 ms	Number of cycles >20,000
	Piezoelectric	BN/PT & MXene/PT	Heterogeneously hierarchical piezoelectric composite [97]	39.3 $\text{mV}\cdot\text{kPa}^{-1}$	30.1 ms	>30 days
	Piezoresistive/Piezoelectric	Polypropylene	Membrane [243]	600 $\text{pC}\cdot\text{N}^{-1}$	-	-
Multiparametric cardiopulmonary monitoring	Piezoelectric	PVDF	Curved structure [138]	0.153 $\text{V}/\text{strain}\%$	-	-
	Piezoelectric	ZnO nanotube/graphene	ZnO nanotube arrays [141]	-4.4 kPa^{-1}	<100 ms	Number of cycles >18,000
	Pyro-piezoelectric	Cellulose nanocrystal	Multilayer structure [142]	0.8 $\text{V}\cdot\text{kPa}^{-1}$	8 ms	Number of cycles >1,000
	Piezoelectric	PZT	Electronic skin [63]	0.018 kPa^{-1}	60 ms	Number of cycles >5,000
	Piezoelectric	FEP	Folded double-layer piezoelectric sensor [143]	3.33 $\text{V}\cdot\text{kPa}^{-1}$	-	Number of cycles >1,100,000
	Piezoelectric	MoS ₂ /PVDF	Nanocomposite fiber sensors [144]	0.22 $\text{V}\cdot\text{kPa}^{-1}$	-	>6 weeks
Multimodal signal fusion	Piezoelectric-like	FEP	Sandwich-structure piezoelectric [176]	4100 $\text{pC}\cdot\text{N}^{-1}$	18.6 ms	Number of cycles >3,600
	Piezoelectric/Ion channel	PVDF/PCTE	Membrane [158]	0.21 $\text{V}\cdot\text{kPa}^{-1}$	20 ms	>10,000 s
	Piezoelectric	PVDF	Filamentary serpentine mesh [65]	0.4 $\text{mV}\cdot\mu\text{E}^{-1}$	-	Number of cycles >10,000
	Piezoelectric	P(VDF-TrFE)/KNN/GR	Composite piezoelectric thin film [157]	430.6 $\text{pC}\cdot\text{N}^{-1}$	-	Number of cycles >2,800

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